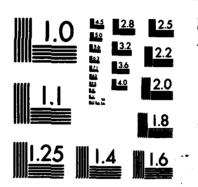
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CORRELATION OF FEDERAL TEST METHOD STANDARD 791B METHOD 354 WITH ARMY 240-HOUR TRACKED VEHICLE TEST CYCLE METHOD 355T

FINAL REPORT AFLRL No. 180

Ву

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U.S. Army Fuels and Lubricants Research Laboratory
Southwest Research Institute
San Antonio, Texas

Under Contract to

U.S. Army Belvoir Research and Development Center Materials, Fuels, and Lubricants Laboratory Fort Belvoir, Virginia

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30 September 1983



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20. ABSTRACT (Continue on reverse side if necessary and identify by block number)

Currently the U.S. Army has two full-scale engine tests which are used for qualifying engine oils. Both tests are based on the Detroit Diesel 6V-53T engine with a number of similarities between the two test procedures. The first of these tests is Method 354, FTMS 791B for qualification of MIL-L-46167 arctic engine oils (OEA) while the other is the newly released Method 355T, FTMS 791B for qualification of MIL-L-2104D tactical engine oils (OE/HDO). One of the main differences between these two test

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procedures is that the Method 354 procedure uses an aluminum engine block which is no longer available from the manufacturer. Other differences are that this method is run for a shorter test duration at a lower engine power output level under steady-state conditions. The unavailability of the cast aluminum cylinder block from the manufacturer and the phase-out of this aluminum engine from the Military inventory means that Method 354 must be updated or replaced. This project was an attempt to develop a correlation between the two test methods by comparing results from Method 355T with results from Method 354 using the lubricants used in developing and standardizing Method 354.

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FOR EWORD

The work reported herein was conducted at the U.S. Army Fuels and Lubricants Research Laboratory located at Southwest Research Institute, San Antonio, Texas, under contract DAAK70-83-C-0070, during the period 5 May 1983 through 30 September 1983. Work was conducted for U.S. Army Belvoir Research and Development Center, Ft. Belvoir, Virginia. Contracting Officer Representative and technical monitor responsibilities were under the Chief, Fuels and Lubricants Division, STRBE-VF, in the Belvoir R&D Center Materials, Fuels and Lubricants Laboratory.

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I. INTRODUCTION

Currently the U.S. Army has two full scale engine tests which are used for qualifying engine oils. Both of these tests are based on the Detroit Diesel 6V-53T engine and there are a number of similarities between the two test procedures. The first of these tests is Method 354, FTMS 791B for qualification of MIL-L-46167 arctic engine oils (OEA) while the other is the newly released Method 355T, FTMS 791B for qualification of MIL-L-2104D tactical engine oils $(OE/HDO) \cdot (1-4) *$ One of the main differences between these two test procedures is that the Method 354 procedure uses an aluminum engine block which is no longer available from the manufacturer. Other differences are that this method is run for a shorter test duration at a lower engine power output level under steady-state conditions.

The unavailability of the cast aluminum cylinder block from the manufacturer and the phase-out of this aluminum engine from the Military inventory means that Method 354 must be updated or replaced. The new Method 355T procedure, which is an outgrowth of the original research which produced the Method 354 test, seemed to be an excellent candidate for use in developing a replacement qualification procedure for the MIL-L-46167 lubricants.

This project was an attempt to develop a correlation between the two test methods by comparing results from Method 355T with results from Method 354 using the lubricants used in developing and standardizing Method 354.

II. PROCEDURES AND TECHNIQUES

Engine tests were conducted according to Method 355T, FTMS 791B using lubricants provided by Belvoir R&D Center. A draft copy of Method 355T is included as Appendix A. The tests were run according to the established

^{*}Underlined numbers in parentheses refer to the references at the end of this report.

procedures except that the power levels used during the tests were reduced. Table 1 summarizes the power levels in the various tests. Reduced power levels were required because it was felt that the lower viscosity arctic oils were less capable of protecting the engine than the MIL-L-2104D products for which this procedure was developed. Various levels of derating (indicated by the percentage values in Table 1) were used for different tests as it became obvious that the "marginal pass" lubricant was having difficulty at higher output levels.

III. TEST LUBRICANTS

Three lubricants were used in this test program. The summarized properties of these lubricants are presented in Table 2. The first lubricant was AL-12271-L, OEA lubricant (Lubricant A). This lubricant performed well in Method 354 tests and is a qualified MIL-L-46167 lubricant. A complete list of lubricant properties can be found in Appendix B along with the complete Method 355T test report for this lubricant.

The second lubricant was AL-12272-L, OEA lubricant (Lubricant B). This lubricant was judged to be borderline acceptable in Method 354 tests and is a qualified MIL-L-46167 lubricant. Lubricant properties are listed in Appendices C and D along with complete Method 355T test reports.

The third lubricant was AL-12186-L, a MIL-L-2104B grade OE-10 reference lubricant (Lubricant C). This lubricant failed to meet Method 354 requirements. Again, lubricant properties are listed in Appendix E along with the complete Method 355T test report.

IV. RESULTS

The results of the four tests are summarized in Tables 3 through 6. The first endurance test (No. 31, Appendix B) was run at 8.4 percent derated horsepower conditions using OEA Lubricant A. Analysis of the results indicates that the lubricant performed very well in the test and exhibited low levels of distress.

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TABLE 1. SUMMARY OF OPERATING HORSEPOWERS

	2200 RPM	2800 RPM	TESTS
Method 354 (100 Hours)		235 (Steady State)	
Method 355T (240 Hours)	265	300	
Method 355T-8.4% (240 Hrs)	243	275	31, 32
Method 355T-21.7% (240 Hrs)	208	235	34, 35

TABLE 2. SUMMARIZED LUBRICANT PROPERTIES

Test Lubricants						
Test	(OEA)	(OEA)	(OE-10)			
Method	A	<u> </u>	<u>C</u>			
D 445	27.81	32.00	33.89			
D 445	6.19	6.37	5.69			
D 2270	182	155	107			
D 92	244	229	221			
D 874	1.51	1.04	1.06			
XRF*	0.88	<0.01	0.50			
XRF	<0.01	0.28	<0.01			
XRF	<0.01	0.10	0.08			
XRF	<0.01	0.09	0.11			
GC**	439	406	379			
GC	448	425	408			
GC	452	437	429			
GC	459	452	451			
GC	0	8	5			
			_			
D 972	9	20	30			
	Method D 445 D 445 D 2270 D 92 D 874 XRF* XRF XRF XRF CC** GC GC GC GC	Test (OEA) Method A D 445 27.81 D 445 6.19 D 2270 182 D 92 244 D 874 1.51 XRF* 0.88 XRF <0.01 XRF <0.01 XRF <0.01 GC** 439 GC 448 GC 452 GC 0	Test (OEA) (OEA) Method A B D 445 27.81 32.00 D 445 6.19 6.37 D 2270 182 155 D 92 244 229 D 874 1.51 1.04 XRF* 0.88 <0.01 XRF <0.01 0.28 XRF <0.01 0.10 XRF <0.01 0.10 XRF <0.01 0.09 GC** 439 406 GC 448 425 GC 452 437 GC 0 8			

^{*}XRF = X-Ray Fluorescence Method **GC = Gas Chromatographic Method

TABLE 3. SUMMARY SHEET FOR TEST NO. 31

Lubricant A, OEA

Test Hours Completed: 240 derated 8.4%

Replaced Liner: None Worst cylinder: 2R

	Avg of Best 5	Worst Cylinder	Avg of all 6
Piston WTD		279	277
Hot Stuck Rings	. 0	Ü	0
Demerits	. 8.2	12.0	8.8
2&3 Ring Face			
Demerits	. 0.75	15.0	3.1
Liner Scuffing, %	. 3.3	4.5	3.5
Liner Scuffing, % by mat	. NR	NR	NR
Port Plugging, %	. <1	<1	<1
Valve Burning	. 0	0	0
Fire Ring End Gap Change, in	0.002	0.008	0.003
Oil Consumption, lbs/hr			_
Fe,ppm,@EOT			

Comments:

- 1. EOT=End Of Test.
- 2. NR=Not Rated.

TABLE 4. SUMMARY SHEET FOR TEST NO. 32

Lubricant B, OEA

Test Hours Completed: 60 derated 8.4%

Replaced Liner: None Worst cylinder: 3R

	Avg of Best 5	Worst Cylinder	Avg of all 6
-		*********	
Piston WTD	197	232	202
Hot Stuck Rings	0	0	0
Fire Ring Face			
Demerits	22.0	72.5	30.4
2&3 Ring Face			
Demerits	22.2	35.6	24.4
Liner Scuffing, %	17.4	100.0	31.2
Liner Scuff,% by mat		100.0	31.0
Port Plugging, %	<1	<1	<1
Valve Burning		0	0
Fire Ring End Gap Change, in		0.008	0.003
Oil Consumption, lbs/hr		-	•
Fe,ppm,@EOT			

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Comments:

- 1. 2L and 3R fire rings collapsed.
- 2. #2 and #4 main bearings worn severely and spalled.
- 3. EOT=End Of Test.

TABLE 5. SUMMARY SHEET FOR TEST NO. 34

Lubricant B, OEA

Test Hours Completed: 240 derated 21.7% Replaced Liner: None Worst cylinder: 3R

	Avg of Best 5	Worst Cylinder	Avg of all 6
Piston WTD	226	266	233
Hot Stuck Rings	0	0	0
Fire Ring Face			
Demerits	17.3	61.3	24.5
2&3 Ring Face			
Demerits	15.5	58.1	22.6
Liner Scuffing, %	22.5	91.0	33.9
Liner Scuff, % by mat	29.1	96.0	40.3
Port Plugging, %	<1	< 1	<1
Valve Burning	0	0	0
Fire Ring End Gap Change, in	0.0	0.007	0.002
Oil Consumption, lbs/hr	0.54		
Fe,ppm,@EOT	110		

Comments:

- Small oil leak during test, impossible to quantify.
 EOT=End Of Test.

TABLE 6. SUMMARY SHEET FOR TEST NO. 35

Lubricant C, OE-10

Test Hours Completed: 20 derated 21.7%

Replaced Liner: None Worst cylinder: 1L

	Avg of Best 5	Worst Cylinder	Avg of all 6

Piston WTD	147	152	147
Hot Stuck Rings	0	0	0
Fire Ring Face			
Demerits	30.0	60.0	35.0
2&3 Ring Face	-		
Demerits	26.1	56.9	31.2
Liner Scuffing,%	42.5	93.0	50.9
Liner Scuff,% by mat	47.6	94.5	55.4
Port Plugging, %	<1	<1	<1
Valve Burning	0	0	0
Fire Ring End Gap Change, in	0.012	0.009	0.011
Oil Consumption, lbs/hr	0.54	•	
Fe,ppm,@EOT	320		

Comments:

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- 1. No.1 ring on 2R collapsed.
- 2. EOT=End Of Test.

The second test (No. 32, Appendix C) was run under the same derated horse-power conditions using OEA Lubricant B. The test completed only 60 hours before severe liner scuffing and bearing distress forced test shutdown to avoid catastrophic failure. Two liners were severely scuffed, and bearing distress was evident throughout the engine. This was judged to be a lubricant-related failure.

The third test (No. 34, Appendix D) again utilized OEA Lubricant B as the test lubricant. This time, however, the horesepower was derated 21.7 percent in order to further lessen the severity of the test. The test ran to completion but exhibited levels of distress which are considered borderline acceptable (by definition) based on field performance.

The fourth test (No. 34, Appendix E) utilized MIL-L-2104B OE-10 reference oil, Lubricant C, and was run at 21.7 percent derated horsepower conditions. The test ran only 20 hours before severe liner scuffing in three cylinders forced test shutdown in order to avoid catastrophic failure. High engine oil iron content was also noted at 20 test hours.

Selected results of these four tests are compared to Method 354 results in Table 7.(5)

V. CONCLUSIONS

These four tests indicate that FTMS 791B Method 355T may adequately distinguish the lubricant quality of MIL-L-46167 OEA lubricants when run at 21.7 percent derated horsepower conditions. The derated Method 355T tests ranked the oils in the same order as past Method 354 tests and field experience. (5-7) Lubricant A performed well at 8.4 percent derated conditions and should continue to do so at 21.7 percent derated conditions. Lubricant B completed the test and exhibited borderline acceptable characteristics (based on scuffing and ring face distress) when run at the 21.7 percent derated conditions. This lubricant was judged a borderline pass in the Method 354 tests. Lubricant C exhibited definite "failure" characteristics (based on failure to complete the test and high distress levels) in both the Method 354 and 355T tests.

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TABLE 7. COMPARISON OF METHOD 354 TESTS TO METHOD 355T TESTS

	OEA LUBRICANT A		OEA LUBRICANT B		OE-10 LUBRICANT C	
Test Method	354	355T	354	355T	354	355T
Test Number	9A	31	8	34	7	35
Hours Completed	100	240	98	240	4#	20
Power Reduction, %	0	8.4	0	21.7	0	21.7
Hot Stuck Rings	0	0	0	Ó	1	Ö
Ring Face Demerits						
Or Burning **	3H3L	3.1	4H2L	22.6	1H5L	31.2
Liner Scuffing, %	27	3.5	46	33.9	20	50.9
Fire Ring End		•				
Gap Change, in x .001	NR	3	NR	2	NR	11
Oil Consumption, lbs/hr	0.46	0.39	0.41	0.54	3.6	0.54
Fe, ppm, @ EOT	NR	20	NR	110	NR	320
Qualitative Judgement	ACC	ACC	BLA	BLA	FAIL	FAIL

Notes:

- 1. EOT=End Of Test.
- 2. NR=Not Rated.
- 3. * This test exhibits low liner scuffing and ring burning due to the low number of hours run prior to catastrophic siezure in 3L.

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- 4. ** For Method 355T tests this is the average of 2&3 ring face demerits. For Method 354 tests H=Heavy, M=Medium and L=light ring face distress, preceded by the number of cylinders exhibiting that level of distress on all compression rings.
- 5. ACC=Acceptable, BLA=Borderline Acceptable.

VI. RECOMMENDATIONS

- Other derated Method 355T tests should be performed using MIL-L-46167 lubricants of proven quality in order to verify the above conclusions and so evaluate repeatability.
- If the derated test continues to successfully discriminate MIL-L-46167 lubricant quality, then pass/fail limits should be established and it should replace Method 354.

VII. REFERENCES

- 1. U.S. Military Specification MIL-L-2104D, Lubricating Oil, Internal Combustion Engine, Tactical Service, April 1983.
- 2. U.S. Military Specification MIL-L-46167, Lubricating Oil, Internal Combustion Engine, Arctic, February 1974; Amendment 1, May 1978.
- 3. Method 354, Federal Test Method Std. 791B, "Performance of Arctic Lubricating Oils in A Two-Cycle Engine Under Steady State Turbosuper-charged Conditions," June 1974.
- 4. Method 355T, Federal Test Method Std. 791B, "6V-53T 240-Hour Tracked Vehicle Cycle Endurance Test Procedure--Performance of Engine Lubricating Oils in A Two-Cycle Diesel Engine Under Cyclic, Turbo-Super-charged Conditions," July 1982.
- 5. S. J. Lestz, "Development of a Diesel Engine Test Technique for Evaluating Arctic Engine Oils," Final Report AFLRL No. 24, AD 768901. Conducted under Contract DAAD05-70-C-0250, September 1973.
- 6. S. J. Lestz and T. C. Bowen, "Development of Army Synthetic Automotive Engine Oils for Arctic Service," AFLRL Interim Report No. 73, AD A019113, September 1975.
- 7. S. J. Lestz and T. C. Bowen, "Army Experience with Synthetic Engine Oils in Mixed Fleet Arctic Service," SAE Paper No. 750685, presented at National F&L Meeting, Houston, Texas, June 3-5, 1975.

APPENDIX A

6V-53T 240-HOUR TRACKED-VEHICLE CYCLE ENDURANCE TEST PROCEDURE

DRAFT

Date 7-15-82

6V-53T 240-HOUR TRACKED VEHICLE CYCLE ENDURANCE TEST PROCEDURE

PERFORMANCE OF ENGINE LUBRICATING OILS IN A TWO-CYCLE DIESEL ENGINE UNDER CYCLIC, TURBO-SUPERCHARGED CONDITIONS

1. SCOPE

- 1.1 This method is used for determining the effect of lubricating oils on wear, ring-sticking, and accumulation of deposits in a reciprocating internal combustion engine. Evaluation is based on: (a) the ability of the test engine to maintain performance throughout the cycle, (b) wear of critical engine components, (c) accumulation of fuel and lubricant related engine deposits, particularly in the piston ring zone areas, and (d) the physical and chemical condition of the lubricant monitored throughout the test.
- 1.2 The test involves the operation of a militarized six-cylinder, fuel injected, turbo-supercharged, 2-stroke-cycle diesel engine under cyclic conditions for a total of 240 hours. Prior to test the engine is reconditioned as described herein. Evaluation is made by comparing the test oil performance to that of a reference oil of known quality.
- 2. SAMPLE
- 2.1 A minimum of 55 gallons of test oil is required.
- 3. APPARATUS
- 3.1 References.
- 3.1.1 Coordinating Research Council Diesel Engine Rating Manual No. 5.
- 3.1.2 Proposed CRC Rating System for Diesel Engine Deposits, CRC, Inc., New York, NY, February 1973. This is a good reference but not mandatory.
- 3.1.3 Detroit Diesel Engine Series 53 Service Manual.
- 3.1.4 Method 346.2 Federal Test Method Standard 791.
- 3.2 Test Engine Systems.
- 3.2.1 Test Engine. A Detroit Diesel 6V-53T Engine (Military Model 5063-5395), is specified for this method, with the following parts:

Quantity	Detroit Diesel Part No.	Item
1	5133512	Flywheel
1	5126671	Scuff Plate
6	9409129	Bolt
1	51014 31	Turbocharger
1	5133427	Heat Exchanger
1	8539 953	Transmission Cooler (8 pl.)
1	8528 885	Oil Cooler (16 pl.)
6	5140949	Connecting Rod
6	5228784	Fuel Injector (M70 or N70)
1	5199793	Overhaul Gasket Kit
8	AC-A86CW	Air Filter
4	5132 924	Hand Hole Gasket
1	AC-T552	Primary Fuel Filter
1	AC-TP540	Secondary Fuel Filter
2	AC-PF132W	Oil Filter
24	5197176	Exhaust Valves
6	5149315	Liner, Piston, Ring Set
6	5109970	Upper Oil Control Ring & Expander

- 3.2.2 Air Intake System. A special air intake system is required for this method. The low temperature air-heater and primer assembly shall be removed from the engine. The air barrel assembly, described in Appendix A, is attached in the horizontal position to the turbocharger compressor.
- 3.2.3 Crankcase Ventilation System. The crankcase breather system described herein shall be used for this method. The breather pipes are joined at a tee connection and connected to a short piece of 1-1/4 inch rubber hose. The total gas flow is then piped by 1 inch conduit to the blowby surge chamber from which the gas passes through a blowby meter and is discharged vertically. Appendix B illustrates the blowby surge tank. The airbox is drained from the left and right airbox drains through #49 orifices and into one gallon collection cans. Filters may be placed before the orifices in order to prevent orifice plugging.
- 3.2.4 Cooling System. The coolant flow shall be from the thermostat housing cover outlet, through a 2 inch diameter transparent section of pipe into the coolant heat exchanger and back to the suction side of the coolant pump. A one-gallon cylindrical surge tank (6-1/2 inches diameter by 8-1/2 inches long) located to the side and above the coolant heat exchanger is provided as a settling vessel to insure coolant deaeration. During test the cooling system is operated with the pressure cap in the vented to atmospheric position. The engine thermostats are blocked in the full-open position for this test. Coolant heat exchanger shall be a BCF American Standard 5-030-06-024-006 or equal. System coolant capacity is six gallons. Coolant flow rate may be measured and reported.
- 3.2.5 Fuel System. The primary and secondary fuel filter assemblies are relocated to a remote position off the engine and away from the heat of the exhaust gas. The same premium grade fuel lines (minimum length) and fittings supplied with the engine must be used when relocating the fuel filters. A water-to-fuel heat exchanger is employed to maintain fuel temperature. All lines must be lagged and secured to protect against vibration damage. Appendix C illustrates the fuel system.

3.2.6 Oil System. The 1/4 inch pipe plug in the front of the oil filter housing shall be removed and a sampling valve installed in its place. The oil filter housing is moved to an off engine location. Appendix D illustrates the oil system. No additional oil cooling is allowed.

3.3 Instrumentation.

3.3.1 Load Measurement. Appropriate engine speed and load-indicating devices, from which observed BHp can be determined, must be used in conjunction with suitable power-absorbing equipment. Engine or dynamometer speed shall be measured with an automatic electric revolution counter with synchronized time or suitable electronic speed measuring device. Accuracy of the load measuring device shall be ± 3 ft-lb.

3.3.2 Flow Measurement.

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- 3.3.2.1 Fuel Flow. Provision shall be made for mass flow fuel measurement with a resolution of ± 0.10 pounds per hour. Average fuel temperature is determined at the fuel measuring device and fuel density is established. The fuel-flow measuring device shall be a properly installed mass flow meter.
- 3.3.2.2 Blowby Flow. Blowby flow is indicated with the equipment described in 3.2.3 and Appendix B.
- 3.3.3 Temperature Measurements. Provisions shall be made for thermocouple installations as shown below (total system accuracy shall be calibrated to ± 2 °F). Thermocouples shall be shielded, and, unless specified, shall be immersed to the midstream.

Variable	Location			
Exhaust gas before turbo- charger	Left and right elbows, 2-3/4 inches from manifold			
Turbocharger exhaust exit	2-1/4 inches from turbocharger exit			
Cylinder jacket coolant-in*	<pre>1.5 inch above the inlet end of water pump inlet</pre>			
Cylinder jacket coolant out*	In 1/2 inch pipe plug hole of thermostat housing deaeration dome			
Oil sump*	Sump drain plug, 2-5/8 inches immersion from wall			
Fuel*	At secondary filter inlet			
Compressor inlet air*	<pre>Inlet air barrel, opposite No. l air filter (see Appendix A)</pre>			
Airbox*	Left rear hand hole cover			
Wet bulb/dry bulb	Near air barrel inlet			

^{*} All temperatures shall be recorded at not more than 2 minute intervals during the test.

3.3.4 Pressure Measurements. Provision shall be made for measuring pressures as follows:

Variable	Location			
Intake air vacuum	After air filters, 4 inches from compressor inlet			
Exhaust back pressure	<pre>In 4 inch line, 3 inches after turbocharger exit</pre>			
Exhaust pressure before turbocharger	Right-hand elbow, 3 inches from turbocharger Y connector			
Compressor discharge	Blower inlet housing (remove 1/4 inch pipe plug)			
Airbox	Left rear hand hole cover			
Oil gallery	Left rear gallery top			
Fuel	Secondary filter outlet			
Barometer	In vicinity			
Blowby	In blowby surge tank			

4. MATERIALS

- 4.1 Fuel. Only fuels approved by the U.S. Army Mobility Equipment Research and Development Command, Energy and Water Resources Laboratory, Ft. Belvoir, Virginia, and meeting the requirements set forth in section 4.1.1, Federal Test Method 346.2, Federal Test Method Standard 791 shall be used for this method.
- 4.2 Reference Oil. Reference engine oil REO-203 is to be used for standardizing engine operation as set forth herein. Orders for reference oil should be made out to Southwest Research Institute, P.O. Drawer 28510, San Antonio, Texas 78284 and sent to the ASTM Test Monitoring Center, 4400 5th Ave, Pittsburgh, PA, 15213, Attn: Mr. P.R. Eisaman for transmittal to the supplier.
- 4.3 Cleaning Compound Special. Gulf H-236 "Stoddard" solvent or Exxon "Varsol" may be used to clean parts as described herein. D-Carb (Dubois Chemicals Co., Cincinnati, Ohio) may be used in vat cleaning the engine block.
- 4.4 Engine Coolant. Engine coolant will consist of a 50/50 volumetric mixture of ethylene glycol base antifreeze* and potable water.

^{*}Prestone--mixing with other types not authorized.

5. PREPARATION FOR TEST.

5.1 Engine Disassembly. A systematic inspection and maintenance of the test engine shall be performed prior to each test run. New engines or engines being used for the first time in this test method and thereafter will be disassembled, reconditioned, and gauged before each test. Regardless of their condition, the following parts shall be replaced with new factory production items:

Piston Assemblies
Piston Ring Sets
Cylinder Liners
Fuel Filters, Oil Filter, and Air Filters
All Gaskets and Seals

The measurements prescribed in Appendix E (BEFORE AND AFTER TEST DATA SHEETS) shall be performed and recorded.

- 5.2 Cleaning Procedure.
- 5.2.1 Engine Block. If the engine is completely disassembled, the block shall be cleaned by spraying with solvent.
- 5.2.2 Aluminum Parts. Aluminum parts will be cleaned by spraying with solvent followed by air drying. If deposits are stubborn, the parts may be soaked in solvent for a period up to two hours at a temperature of 100°F or less. The solvent soak must be followed by a warm water wash and air drying.
- 5.2.3 Steel Parts. All steel parts (i.e., rocker arm covers, oil pan, oil heat exchanger, cylinder head decks, oil pump, crankshaft, etc.), shall be cleaned by spraying with solvent, air dried and lightly coated with reference oil.
- 5.2.4 Fuel Injectors. The fuel injectors are removed but not disassembled or adjusted. Only the tips should be lightly wire brushed to remove carbon particles. Should the operation of the engine indicate that their condition might be at fault, the units should be tested, adjusted, and/or replaced with new units.
- 5.2.5 Combustion Chambers and Valves. Exhaust valves are removed and the entire combustion chamber area of each cylinder is cleaned by wire brushing. Valves are only lightly refaced, if inspection shows pitting. Where the sealing surfaces (faces) are not pitted, the valves need be only lightly lapped prior to reassembly. If light refacing does not correct the seating condition, the valve shall be replaced. Regardless of their condition, valves should be replaced after three tests.
- 5.3 Engine Disassembly. The engine block is fitted with new parts as listed in sections 3.2.1 and 5.1. Complete measurements of the block bore, liners, pistons, rings, connecting rod journals, main bearing journals, connecting rod bearing inserts, and main bearing inserts are made prior to each rebuild. Connecting rods and piston pins will be inspected and replaced if not in good service conditon. In addition, camshaft journals to bearings and oil pump clearances shall be checked against service limits during major

rebuilds. These parts will be replaced as required to maintain service limits. The liner outside surfaces contacting the block bore shall be lightly coated with grease to reduce interface fretting corrosion. Other parts shall be coated with reference oil during assembly. Piston pin retainers shall be checked for leakage with KENT MOORE tool number J-23987-01.

5.3.1 The following critical rebuild measurements shall be maintained during engine assembly:

Engine Part	Tolerance or Clearance (1) - Inches
Crankshaft main bearing clearance	0.0010-0.0040
Camshaft bearing clearance	0.0045-0.0060
Connecting rod bearing clearance	0.0011-0.0041
Crankshaft end-play	0.0040-0.0110
Cylinder block bore	
Taper	0.0015 max
Out-of-round	0.0015 max
Inside diameter	4.3565-4.3575 new
Clearance liner to block	0.0005-0.0025
Cylinder liners (installed)	
Taper	$0.0015 \max_{(2)}^{(2)}$
Out-of-round	0.0015 max ⁽²⁾
Inside diameter	3.8752-3.8767
Piston to liner fit	0.0061-0.0098
Piston skirt O.D.	3.8669-3.8691
#1 Fire Ring	
End gap	0.020-0.046
Side clearance	0.003-0.006
#2 Compression ring	
End gap	0.020-0.036
Side clearance	0.007-0.010
#3 Compression ring	
End gap	0.020-0.036
Side clearance	0.005-0.008
#4 Compression ring	
End gap	0.020-0.036
Side clearance	0.005-0.008
#5, 6, 7, Oil rings	
End gap	0.010-0.025
Side clearance	0.0015-0.0055

KASASISIN PIZZEKZAO PIZZEKZAO PISEKSINO PISEKSIO KONSKASKIO PAKOSKANO PARKIZA KZEKZAO POSEK

- 6. ENGINE CONDITIONING AND CALIBRATION PROCEDURES
- 6.1 Engine start-up and shut-down procedures.

⁽¹⁾ All tolerances and clearances given in inches.

⁽²⁾ Using new cylinder liners in a used block.

^{5.3.2} Engine assembly shall be in accordance with TM 9-2815-212-35 and the Detroit Diesel Engine Series 53 Service Manual. Reference must be made to these documents to determine the proper bolt torques, tightening sequences, and final injector timing and valve lash settings. Upper oil control ring expander accompanying DD part number 5109970 shall be installed in place of expanders accompanying liner-piston-ring set.

- 6.1.1 Engine Start-up Procedure. From a cold start, idle the engine for five minutes. Then warm up at 1200 rpm and 88 lb-ft dynamomter load (20 BHp) until oil sump temperature reaches 180°F and coolant jacket-out temperatures reach 170°F. If the coolant system was drained at the previous shut-down, warm up at 1100 rpm and 72 lb-ft load (15 BHp) to insure deaeration of the coolant system. If the engine is started warm and the 180°F oil sump and 170°F coolant jacket-out temperatures are achieved, it is permissible to gradually accelerate the engine without delay to test conditions. The automatic controller set point for coolant-out temperature must remain at 170°F during all startups except when the test is being resumed at the idle modes described in 7.5.
- 6.1.2 Engine Shut-Down Procedure. To shut down the engine from test conditions, slowly bring the engine to idle by turning the rack setting to the idle position. Allow the engine to idle for five minutes and then shut-down by actuating the idle cut-off. The automatic controller set point for coolant out temperatures must remain at 170°F during all shut-downs.
- 6.2 Engine Run-In Procedure.

- 6.2.1 Oil Charge. Charge the engine oil sump with approximately 24 quarts of reference oil. Disconnect the turbo oil supply line at the turbo and crank the engine with the governor control in the fuel cut-off position until one pint of oil is pumped from the disconnected line. Reconnect the turbo line and crank the engine until the oil pressure stabilizes.
- 6.2.2 Operating Conditions. Start the engine in accordance with 6.1.1 and conduct the engine run-in according to the following schedule:

Dynamometer Load, 1b-ft	Power, Obs BHp	Time, min.
88	30	15
310	130	30
420	200	30
422	225	30
	88 310 420	Load, 1b-ft Power, Obs BHp 88 30 310 130 420 200

Coolant jacket-out temperature is maintained at $170 \pm 2^{\circ}F$, and oil gallery pressure is 30 psi minimum. Coolant system deaeration (air free sight glass) must be established by the time the 2500 rpm sequence is completed.

- 6.3 Interim Settings and Adjustments.
- 6.3.1 Immediately following the run-in, check, adjust and record the governor settings. Set the idle speed at 650-700 rpm maintaining a minimum of 5 psi gallery oil pressure. No-load speed maximum should be 2950-3030 rpm, and is adjusted per the Detroit Diesel Series 53 Service Manual.
- 6.3.2 Shut down the engine according to 6.1.2.
- 6.3.3 Five minutes after shut-down, check and reset the injector timing and exhaust valve clearance as follows:

Injector timing - 1.4600 ± 0.0035 inch
Valve clearance - 0.023 to 0.025 inch (hot)

6.4 Initial Power Calibration Check. Full-rack power calibration checks are made in order at 2200, 2500, and 2800 rpm. Engine start-up is in accordance with 6.1.1. The engine is operated at the specified speed until the observed output has stabilized. A coolant jacket-out temperature of 170° ± 2°F is maintained through calibration checks. The parameters shown below must be within specified limits.

Calibration Parameter	2200	2500	2800
Minimum Observed Output, 1b-ft (Bhp)	566(237)	557(265)	529(282)
Normal Oil Gallery Pressure, psi		- 40-60 -	
Minimum Oil Gallery Pressure, psi	30	30	30
Minimum Air Box Pressure, psi	2-2.5	2.5-3.9	2.9-4.4
Maximum Air Inlet Restriction, in. H ₂ 0	. 4	5	8
Maximum Blowby Pressure, in. H ₂ 0	3	3.5	4
Maximum Exhaust Back Pressure, 2in. Hg	2.1	2.7	2.7
Normal Fuel Pressure, psi		- 45-70 -	
Minimum Fuel Pressure, psi		- 35	

- 6.5 Shake-Down Run. Immediately following the 2800 rpm power calibration check, the engine is operated for a period of five hours at 2800 rpm and 469 lb-ft dynamometer load (250 BHp) maintaining a coolant jacket-out temperature of 170 \pm 2°F. The test parameter data listed in 7.12.1 shall be recorded hourly during the shake-down run.
- 6.6 Final Power Calibration Check. Following the shake-down run, full-rack power calibration checks shall be made in accordance with 6.4. On completing the 2800 rpm power check, the engine will be shut-down in accordance to 6.1.2 and an airbox inspection performed (see 7.9).
- 6.7 Oil Flush Run. Drain the reference oil and add 20 quarts of test oil. Run the engine for 30 minutes at 1200 rpm and 30 lb-ft load. Oil flush is not necessary if the test oil is the reference oil.

7. TEST PROCEDURE

- 7.1 Oil Drain. After oil flush shut-down, and while the oil is still warm, drain the oil and remove the oil filter. Perform the initial airbox inspection.
- 7.2 Oil Charge. Weigh-in a new oil filter and sufficient test oil to bring the sump level to the full mark on the dipstick gage (approximately twenty-four quarts). Crank the engine long enough to stabilize the oil pressure (approximately 10 seconds), wait five minutes and recheck the oil level.
- 7.3 Full Load Performance Determination. Conduct a full load (full rack) performance determination measuring engine dynamometer load, brake horsepower (BHp), and brake specific fuel consumption (BSFC) at 200 rpm intervals between engine speeds of 1800 and 2800 rpm. Record all data as per 7.12.1.

7.4 Test Duration. The test consists of 240 hours of operation at prescribed test conditions. Interim oil adjustments, airbox inspections, and oil samplings are made on the following schedule:

Operation	0	20	40	60	80	100	120	140	160	180	200	220	240
Oil Adjustments	_	$\overline{\mathbf{x}}$	$\overline{\mathbf{x}}$	$\overline{\mathbf{x}}$	$\overline{\mathbf{x}}$	X	$\overline{\mathbf{x}}$	X	X	X	X	$\overline{\mathbf{x}}$	
Oil Sampled	X	X	X	X	X	X	X	X	X	X	X	X	X
Airbox Inspected	X	-	_	X	_	_	X	-	-	X	_	_	_
Oil Change	X	_	_	_	_	_	X	_	_	_	_	-	-
Air Filter Change	-	_	_	-	_	-	*	-	-	-	-	-	_

X indicates adjustment, sampling or inspection to be performed at given test time.

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7.5 Test Cycle Description. The endurance test consists of repeating a four-mode, five-hour operating cycle four times daily for a total of 20 hours. The engine is then shut down for a period of four hours after which the daily cycle is repeated. The five-hour operating cycle (shown below) consists of: 0.5 hour at engine idle followed by 2.0 hours at maximum power, followed by 0.5 hour at engine idle followed by 2.0 hours at maximum torque. The 20-hour endurance cycle is conducted for 12 days without interruptions longer than three days.

Endurance Test Operating Cycle

					Jacket-Out
Period	Mode	Time, hrs	Load, %	Speed, rpm	Temp, °F
1	Idle	0.5	0	675 ± 10	110
	Max Power	2	100	2800 ± 10	170
	Idle	0.5	0	675 ± 10	1 υ
	Max Torque	2	100	2200 ± 10	170
2	Idle	0.5	0	675	110
	Max Power	2	100	2800	170
	Idle	0.5	0	675	110
	Max Torque	2	100	2200	170
3	Idle	0.5	0	675	110
	Max Power	2	100	2800	170
	Id le	0.5	0	675	110
	Max Torque	2	100	2200	170
4	Id1e	0.5	0	675	110
	Max Power	2	100	2800	170
	Idle	0.5	0	675	110
	Max Torque	2	100	2200	170
5	Shutdown	4	0	0	

7.6 Operating Conditions. The engine shall be operated under the following conditions:
Limits

		DIMITO	
	Max	Max	
Operating Condition	Power Mode	Torque Mode	Idle Mode
Speed, rpm	2800 ± 10	2200 ± 10	675 ± 10
Fuel Flow, 1b/hr	117 min.	96 min.	NS
-			

^{*} As needed.

		Limits	
	Max	Max	
Operating Condition	Power Mode	Torque Mode	Idle Mode
Obs BHp Output	300±5	265±5	NS
Jacket-out, °F	170 ± 2	170 ± 2	110 ± 5
Coolant AT, °F	8 - 12	8 - 12	2 - 6
Inlet Air, °F	90 ± 5	90 ± 5	90 ± 5
Oil Sump, °F	250 max	250 max	NS
Fuel Temp at Filter	95 ± 5	95 ± 5	ns
Fuel Pressure, range	35 - 70	35 - 70	ns
Compressor Suction, clean			
filter, inches water	8.0 max	NS	ns
Compressor Suction, dirty			
filter, inches water	10.0 max	NS	NS
Exhaust Back Pressure (after			
turbo), inches Hg max	2.7	2.1	NS
Blowby Pressure, inches water	4.0 max*	NS	NS
Oil Pressure, psi	30 min	30 min	5 min

^{* =} Blowby pressure greater than 4 inches of water constitutes test shutdown for inspection.

7.8 Oil Adjustment and Oil Change.

- 7.8.1 Shut down the engine according to 6.1.2. Note that oil samples must be taken during the 5 minute idling period (see 7.7).
- 7.8.2 Make oil adjustments according to the schedule of 7.4 by adding a weighed amount of test oil to the sump, bring the level to the full mark on the dipstock. Maintenance of an oil log sheet is required. If the oil level is below add halfway (10 hours) through the period, weight and add roughly a gallon of oil so that the engine can finish the period safely. If oil temperature exceeds 250°F, remove and clean the oil heat exchanger. Oil consumption should not exceed 0.75 lb/hr or the test shall be considered invalid.
- 7.8.3 After the 120-hour oil sample is taken, the engine is shutdown according to 6.1.2. The oil is drained from the oil filter housing and the engine crankcase. A new charge of test oil and a new oil filter are installed per 7.2. The air cleaners are also changed at this time.
- 7.9 Airbox Inspections. Four airbox inspections shall be made as specified in 7.4. The zero-hour inspection is made at the completion of the final power check and prior to the installation of test oil. Observations made at each airbox inspection must be recorded and included in the final engine inspection. The areas inspected, performance levels noted and means of inspection shall be as follows:

NS = Not Specified

^{7.7} Used Oil Sampling. Take a 8 fluid ounce sample of oil at the oil filter housing according to the schedule specified in 7.4. This is done with the engine idling prior to the scheduled shut-down and oil adjustment. If fuel dilution (greater than 5%) is detected in the oil, the fuel leak should be repaired and the oil changed before the test continues.

Area Inspected	Performance Level Noted	Means of Inspection
Inlet Ports	Percent Plugging	Visu al
.Piston Skirt	Tinplate melting Scoring Burning	Visual
Ring Lands	Carbon Deposits	Visual
Rings	Freedom Face Scuffing	Blunt Probe and Visual
	Face Burning	VISUAL
Cylinder Liner	Scuffing(1) Scoring Bridge Cracking(2) Glazing	Illuminated and Magnifying Borescope Visual

⁽¹⁾ Scuffing shall be described in terms of degree (light, medium and heavy) and in terms of area (thrust, anti-thrust, front and rear). Severe scuffing constitutes a test shutdown.

- (2) Bridge cracking constitutes a test shutdown.
- 7.10 Full Load Performance Determination. Immediately following the final endurance cycle, conduct a full load (full rack) performance determination in the same manner as described in 7.3 (Before Test).
- 7.11 Final Oil Drain. Shut down engine as outlined in 6.1.2. Let the engine stand for five minutes, then drain the crankcase and oil filter housing. Weigh and record the quantity of oil drained, the oil filter, and the blowby can.
- 7.12 Data Recording.
- 7.12.1 The following data shall be recorded once during each idle mode and twice during each power and torque mode.

Operator Date Time Test Hours Engine Speed, rpm Load, 1b-ft Fuel Rate, 1b/hr BSFC, 1b/bhp-hr Observed Output, BHp Temperatures, °F Exhaust Manifolds Turbocharger exit Coolant jacket-in Coolant jacket-out 011 Sump Fuel at Filter Compressor Inlet Air Airbox Ambient Air (wet/dry bulb) Pressures

Intake vacuum, in. H₂0
Exhaust Turbocharger exit, in. Hg
Exhaust Manifolds, psi
Compressor Discharge, psi
Blower Discharge (Airbox), psi
Transfer pump, psi
Oil Gallery, psi
Blowby, in. H₂0
Barometer, in. Hg.

- 7.13 Problems Encountered During Test.
- 7.13.1 High Blowby. Blowby pressure greater than four inches of water constitutes test shutdown for inspection. If the problem appears to be caused by lubricant-related ring wear, then the test should be terminated. Severe problems may be present at blowby pressures less than four inches of water.
- 7.13.2 Liner Scuffing-Ring Wear. Liner scuffing-ring wear is generally accompanied by high blowby pressures. This condition generally requires test termination. In the case that, before 41 test hours, one liner exhibits severe scuffing while all others exhibit normal wear, that liner-piston-ring set may be replaced and the test continued. The removed parts should be rated but not included in reported averages. Removed liners should exhibit 30% or greater overall scuffing. A fresh oil charge may be used in this instance. Appropriate notations should appear in the test report. Engine oil iron content is also a good indication of ring wear and scuffing.
- 7.13.3 Visually Observed Scuffing. If severe liner scuffing is observed during the airbox inspections, and that scuffing is judged to be of a progressive nature, then the test should be terminated. Severe liner scuffing can lead to liner o-ring melting and subsequent catastrophic engine failure. Progressive liner scuffing is generally accompanied by high blowby and rapidly increasing engine oil iron content.
- 7.13.4 Fuel Dilution. If a fuel concentration greater than five percent by weight is detected in the lubricant, the fuel leak should be repaired and the oil changed before the test continues. Fuel crossover lines are generally at fault in this case. Appropriate notations should appear in the test report.
- 7.13.5 Coolant Dilution. If coolant is detected in the lubricant, the leak should be repaired and the oil changed before the test continues. Appropriate notations should appear in the test report. In order to avoid coolant dilution when cylinder heads are removed the following procedure should be used;
 - 1. Drain lubricant.
 - 2. Drain coolant.
 - Perform desired work taking care to minimize coolant drainage into sump.
 - 4. Flush oil passages by pouring new oil down exposed oil drain holes.
 - 5. Reinstall head(s).

- 6. Refill with original oil.
- 7. Refill coolant system.
- 7.13.6 High Oil Temperature. Oil sump temperatures greater than 250°F generally indicate that the oil-water heat exchangers need cleaning. If after cleaning, the sump temperature remains high, then the test should be halted until the problem is corrected.
- 7.13.7 Loss of Power.

- 7.13.7.1 Faulty Injectors. Poor engine performance during the test may be caused by worn, sticking, broken or leaking injectors. Injectors may be replaced at any point in the test.
- 7.13.7.2 Valve Distress. Poor engine performance caused by exhaust valve distress (burning) constitutes test termination. No exhaust valve replacement is allowed. Exhaust valve stem breakage constitutes test termination, but is not considered lubricant-related failure.
- 7.13.7.3 Mechanical Problems. Poor engine performance caused by faulty turbochargers, blowers, misadjusted injectors, etc., may be corrected by component replacement and/or adjustment. Appropriate notations should appear in the test report.
- 7.13.8 High Oil Consumption. High oil consumption (0.75 lb/hr) is generally caused by cracked piston pin retainers or worn oil control rings. Cracked piston pin retainers may be replaced at any point in the test. One set of oil control rings may be replaced before 40 hours of test operation if they appear to be wearing abnormally and causing high oil consumption. If the average oil consumption during the test is greater than 0.75 lb/hr, the test will be considered invalid.
- 7.13.9 Leaks. Lubricant or coolant leaks should be corrected during the course of the test.
- 8. EVALUATION OF RESULTS
- 8.1 Part Ratings.
- 8.1.1 Preparation for Rating. Pistons and cylinder liners are removed from the engine. Care must be taken to avoid disturbing engine deposits during disassembly. Pistons and cylinder liners are numbered on the thrust side. Using a hydraulic press, split the cylinder liners in half along a longitudinal plane separating the thrust and anti-thrust sides. Any engine not completing the full 240-hour test must be inspected for signs of misassembly before a failure may be termed "lubricant-related."
- 8.1.2 Piston Ratings. Using the terminology of 8.1.5, the CRC Diesel Engine Rating Manual No. 5, and the proposed CRC Rating System for Diesel Engine Deposits (First Draft), rate the pistons for the following:

Ring groove carbon filling, % ring supporting carbon, and Weighted Total Demerit (WTD)

Skirt lacquer
Ring sticking
Oil Control Ring Groove Lacquer
Ring Face Condition

8.1.3 Cylinder Liner Ratings. Using the terminology of 8.1.5 and CRC Diesel Engine Rating Manual No. 5, rate the cylinder liners for the following:

Leavestan Whiteham Falletan

Intake Port Restriction
Scuffing (percent fire ring travel area)
Glazing (percent fire ring travel area)
Lacquer

- 8.1.4 Other Ratings. Combustion chamber deposits in the cylinder head and in the piston crowns shall be rated in terms of texture and depth. Exhaust valves, camshaft lobes, rocker arms, tappets/roller-followers, exhaust valve bridges, crankshaft journals and main/connecting rod bearing inserts will also be rated. Crankshaft main bearing journals and bearings need only be rated at major rebuilds. Any unusual deposits or part condition shall be noted.
- 8.1.5 Rating Terminology. Ratings shall be made using the CRC Diesel Engine Rating Manual No. 5 and terminology defined as follows:

<u>Scuffing</u> - Mechanical disturbance of a rubbing surface with no appreciable surface roughness to feel.

Scoring - Mechanical disturbance of a rubbing surface with a definite surface roughness in line with motion characterized by the transfer of metal by dragging which results in progressive deterioration.

<u>Seizure</u> - Sticking together of two surfaces characterized by the presence of small particles of material which have become welded to the surface.

Glazing - Continuous removal of surface material resulting in a mirror-polished appearance of very low micro-finish.

Burning - Removal of metal from sealing surface (ring face) to form leakage paths.

Lacquer - A thin varnish-like deposit which cannot be removed by wiping with saturated solvents, such as petroleum naphtha, but is soluble in lacquer solvents, such as benzene and acetone.

<u>Carbon</u> - A firm deposit composed primarily of hydrocarbon residue which has thickness, volume and texture (hard, medium, and soft).

Ash - Residue of combustion, inorganic in nature.

Ring Sticking - The relative degree of freedom of a piston ring in its groove as removed from the engine.

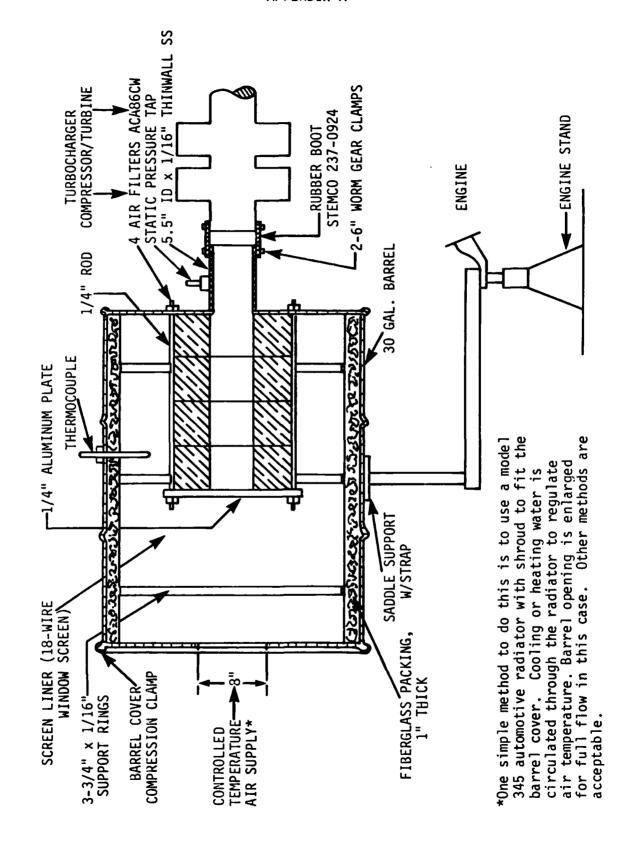
- 8.2 Lubricant Analyses. Test lubricant degradation over the 240-hour test period shall be determined and reported as shown in Appendix G.
- 8.3 Data Presentation.
- 8.3.1 Rating Data. Suitable forms for recording data are shown in Appendix F; all information shown on these forms shall be furnished with the test report.
- 8.3.2 Operating Data. Mean and standard deviation operating data for the maximum power mode and the maximum torque mode shall be reported, together with the average oil consumption. Plotted full-load power performance data before and after test will be included. This will show BHp, BMEP, and BSFC at full rack plotted as a function of engine speed.
- 8.3.4 Build-up and Wear Measurement Data. Suitable forms for presenting the build-up and wear measurements are presented in Appendix H.
- 8.3.5 Photographic Data. Color photographs of each piston and split cylinder liner showing both thrust and anti-thrust sides shall be presented. All photographs shall be on a white background and shall be clearly marked giving cylinder number, right or left, and thrust or anti-thrust. Photographs of piston ring surfaces (opposite gap) and cylinder head deposits shall also be presented. Pictures shall be presented in the following order and manner:
 - 1. Piston rings 1-L and 1-R shall be on the same page. Apparent ring diameter shall be equal to or greater than four inches. Rings shall be photographed with a space between each ring and in the top to bottom order of 1,2,3,4,5,6,7. Lighting should emphasize ring distress and attempts should be made to eliminte extraneous reflections from the ring surfaces.
 - 2. Piston 1-L thrust and antithrust shall be presented on the same page. Apparent piston height shall be equal to or greater than 4 inches. The thrust photograph should be the left most of the two photographs in all instances.
 - 3. Piston 1-R thrust and antithrust shall be presented on the same page.
 - 4. Liner 1-L thrust and antithrust shall be presented on the same page. Apparent liner height shall be equal to or greater than six inches.
 - 5. Liner 1-R
 - 6. Rings 2-L and 2-R
 - 7. Piston 2-L
 - 8. Piston 2-R
 - 9. Liner 2-L
 - 10. Liner 2-R
 - 11. Rings 3-L and 3-R
 - 12. Piston 3-L
 - 13. Piston 3-R
 - 14. Liner 3-L
 - 15. Liner 3-R
 - 16. The left and right cylinder heads shall be displayed on the same page. Apparent head length shall be equal to or greater than five inches. Heads shall be displayed horizontally with cam followers topmost. Combustion chambers should be labeled 1R, 2R, etc.

9. PRECISION

9.1 A reference test is required when a new engine or a new test stand is put into service for the first time, or when an established facility re-installs a test stand. To maintain severity level, reference tests on each engine are required every thirteen tests. This implies that twelve candidate oils may be tested between reference runs on a single engine. An engine is defined as a block and any buildup constitutes a test. Each test stand must be referenced every ninth test or six months, whichever comes first. This implies that each stand may run eight candidate oils between reference tests or that six months may elapse between reference runs. Reporting of an engine's or stand's reference history is optional.

APPENDICES

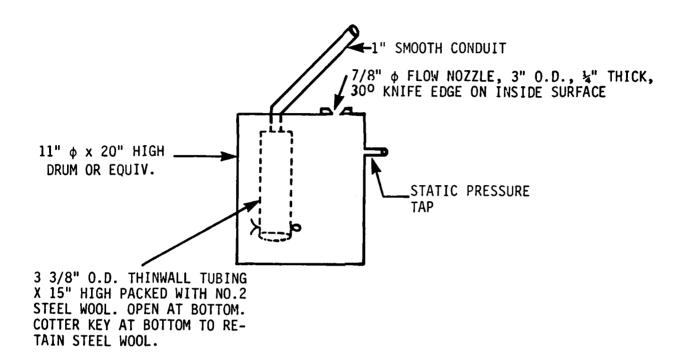
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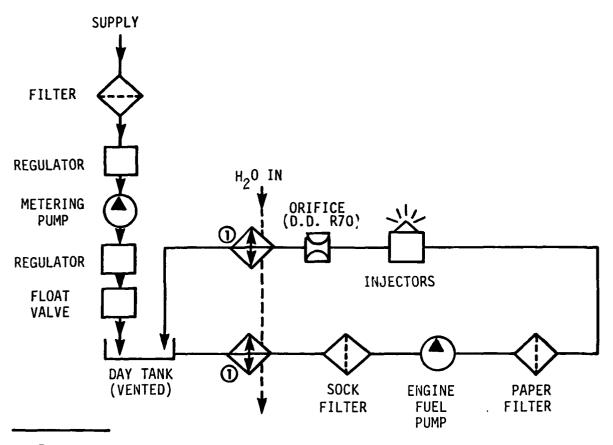
TOWN RECORD DEPOTE NEEDEN DESCRIPTION DESC

APPENDIX B

BLOWBY SURGE TANK



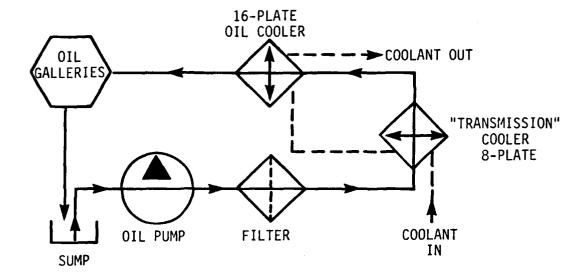
APPENDIX C FUEL SYSTEM SCHEMATIC



① AMERICAN STANDARD BCF 5-030-03-014-003 HEAT EXCHANGERS OR EQUIVALENT

APPENDIX D

OIL SYSTEM SCHEMATIC



APPENDIX E

BEFORE TEST AND AFTER TEST

TEST NO.	
BLOCK NO	
HEAD NO	L
	R
DATE STARTED	
DATE FINISHED	
LUBRICANT	
FILET.	

DATE	TEST NO	•	TECHNICIAN
TUDDIOAM	DUST		

6V53T PISTON RING CLEARANCES

		BEFORE TES	<u>T</u>	AFTER TEST			BEFORE TEST		AFTER TEST
		End Gap*	<u>Side</u>	End Gap			End Gap	Side	End Gap
1L	1 _	-		ļ <u>.</u>	1R	1			
	2 _					2			
	3 _					3			
	4 _					4			
	5					5			
•	6 _					6			
	7 _					7			
2L	1				2R	1			
	2					2			
	3					3			
	4					4			
	5					5			
	6					6			
	7 _			_		7			
3L	1				3R	1			
	2					2			
	3					3			
	4		_			4			
	5					5			
	6					6			
	7					7			

Build-Up Engine Measurement Specifications (inches)

	End Gap	Side Clearance
No. 1, Fire Ring	0.020-0.046	0.003-0.006
No. 2, Compression Ring No. 3 & 4, Compression Rings No. 5, 6 & 7, Oil Rings	0.020-0.036 0.020-0.036 0.010-0.025	0.007-0.010 0.005-0.008 0.0015-0.0055

^{*}All end gap measurements taken in 3.8750" I.D. measuring jig.

DATE		TEST NO	ТЕСН	N]CIAN
	LUBR	ICANT	FUEL	
	6 V 5	3T CYLINDER LINER INSIDE	DIAMETER (INSTALL	ED)
Meac		at 3.8750 inches.	(4.01.02	
	_	en thousandths of an inch	_	
			•	
		BEFORE TEST Top * Middle* Bottom		AFTER TEST Middle Bottom
• •			"	Modie Boccom
1L	T - AT		-	
	F - B		-	
2L	T - AT		-	· ·
	F - B		-	<u> </u>
3L	T - AT		-	
	F - B		-	
1R	T - AT		1	
	F - B		-	
2R	T - AT			
	F - B			
3R	T - AT			
	F - B			
			II	
* 5/8	" 5" and Q" ba	low block surface, respecti	1	
5,0	, , and , be	now block surface, respecti	vely.	
	•			
			t	
Build	-Up Engine Mezs	surement Specifications (i	nches)	
	der Liners (ins	· · · · · · · · · · · · · · · · · · ·	-	
Taper		0.0015	Max	
Out-o	of Round	0.0015		

3.8752-3.8767

Inside Diameter

DATE	TEST NO	TECHNICIAN .
1 HDDI CANT	Fi	IFI

BEFORE TEST

6V53T PISTON - CYLINDER LINER CLEARANCE

All measurements are in inches unless otherwise indicated.

	CYLINDER LINER I.D.		PISTON SKIRT O.D.	CLEARANCE	
	MIN.	MAX		MIN.	MAX
1L		d	ii	ii	
2L				<u> </u>	ļ
3L				<u> </u>	
1R		·			.
2 R					
3 R					

Build-Up Engine Measurement Specifications (inches)

0.0061-0.0098
0.38669-3.8691
3.8752-3.8767

DATELUBRICANT		TEST NO		TECHNICIAN_			
				FUEL_			
		6V53T	PISTON PIN 1	TO PISTON BUSH	IING CI	LEARANCE	
		BEFORE TE	ST		•	AFTER TE	ST
	PIN	BUSHING	CLEARANCE		PIN	BUSHING	CLEARANCE
lL							
2L							
3L							
lR							
2 R							
3R							
	DTM	BEFORE TE		O ROD BUSHING		AFTER TE	ST CLEARANCE
lL	PIN	BUSHING	CLEARANCE		LIM	BOSHING	CLEARANCE
L 2L							
3L							
1R							
2R						 .	
2 R 3 R							
JK							
Rebuil	ld Eng	ine Measure	ment Specificat	ions (inches)			
Pistor	n Pin	Outside Dia	meter			746 - 1.37	
		ing Inside				775 - 1.37 025 - 0.00	
		on Bushing				760 - 1.37	
	_	Inside Dia Bushing Cle)10 - 0.00	

MARKET PROGRAMME BENZZZZEN BENZZZZEN BENZENSKE BENZZZZZEN BENZENSKE BENZZZZZEN BENZZZZZEN BENZZZZZEN BENZZZZZZ

Pin-to-Rod Bushing Clearance

DATE	TEST NO.	TECHNICIAN
LUBRICANT	FUEL	

6V53T BLOCK BORE DIAMETER

Measuring Gauge Set at 4.3560 inches.

Numbers given are ten thousandths of an inch.

T-AT			BEFORE TEST	AFTER TEST
F - B Top Bot	lL	T-AT	Top *	
Bot			Bot **	
Bot		F - B	Тор	
T-AT				
F - B Top Bot Bo	2L	T-AT		
F - B Top Bot Bo			Bot	
Bot		F - B		
Bot				<u> </u>
Bot F - B Top Bot	3L	T-AT		
F - B Top				
Bot		F - B		
Bot				
Bot	LR	T-AT		
F - B Top				
Bot		F - B		
2R T-AT Top				
Bot	2R	T-AT		
F - B Top				
Bot		F - B		
1 1				
2V V-V* 10h	3R	A-AT	Тор	
Bot				
F - B Top		F - B		
Bot				
Build-up Engine Measurement Specifications (inches)	3uilo	i-up Engi		nches)
Block Bore				

0.0015 Taper Max *7 1/2" below block surface **8 1/2" below block surface Out-of Round 0.0015 Max'

4.3565-4.3575 New Inside Diamenter

4.3595 Max

DATE	·	TEST NO		TECHNICIAN	
Ll	JBRICANT		FUEL_		
	6V53T V	ALVE DEPTH (BEFORE	TEST)		
	LEFT SIDE			RIGHT SIDE	
1L			1R		
				· · · · · · · · · · · · · · · · · · ·	
2L			2 R	· · · · · · · · · · · · · · · · · · ·	
3L			3R		
	CRANKSHAFT	THRUST WASHER THIC	KNESS (E	BEFORE TEST)	l
	1				
ONLY	2				
ILD	3				
REBL	4				
MAJOR REBUILD ONLY	Crankshaft	End Play (Before To	est)		
MA.	Oil Pump Cl	earances (Before To	est)		
	Clearan	ce Between Rotors_			
	Clearan	ce Between Rotor a	nd Housi	ng	

Build-Up Engine Measurement Specifications (inches)

Valve Head Relation to Cylinder Head

Surface
Crankshaft Thrust Washer Thickness
Crankshaft End Play
Oil Pump Clearance Between Rotors
Oil Pump Clearance Between Rotor and Housing
O.0010 to 0.0035

		LUBRICANT		···	FUE	L				
	6V53T	MAIN BEARIN	G SHELL AND BEA	RING JOU	RNAL DI	AMETERS AN	D CLEARA	NCES	•	
	Bearin	BEFORE TEST g Journals	Bearing Shells	Clear	AFTER TEST earances Bearing Journals Be				earing Shell	
	A*	B	F BA	Min.	Max		В		ВА	
1										
2										
3										
4										
			arallel to weig							
B:	Microm	eter anvil p	erpendicular to	weights	. В	A: Back				
	6V53T	CONNECTING R	OD BEARING SHEL	L AND BE	ARING J	OURNAL DIA	METERS A	ND CLEARA	NCE S	
	Resti	BEFORE TEST	Bearing Shells	Clear	ances	AFTE Bearing 1	R TEST	Bearing	Shel	
			F BA		Max	A				
1 L								•		
2L										
3L										
J										
1R		· ·								
2R										
3R				-						
Bu	ild-Up	Engine Measur	rement Specifica	tions (in	che s)	<u>NEW</u>		LIMIT		
		ing Journal I			3.49	90 to 3.500	. 00			
Ma		ing Shell Ins rtical axis)	side Diameter		3.50	30 to 3.504	,0			
Ma		•	Journal Clearan	ce	0.00	10 to 0.004	0.0	0060		
		_	g Journal Diamet			90 to 2.750				
	nnectin		g Shell Inside D			611 to 2.750				
Co		g Rod Bearing	Shell to Journ	al	0.00	011 to 0.004		0060		
	Ole	arance		A-29	0.00	11 to 0.00	,1 0.0	3000		

		TEST NO.	TECHNICI	AN				
	LUBRICA	NT	FUEL					
	6V53T	Camshaft Bearing Shell and Bearing Shell Measuring G	_					
ONLY		LEFT CAMSHAFT						
	DEEODE 1	TECT	APPER TROM					
REBUILD	BEFORE 7		AFTER TEST					
	ournal	Bearing	Journal	Bearing				
1								
- 1 ^	 - 							
3								
4								
		RIGHT CAMSHAFT						
1	BEFORE 3	RIGHT CAMSHAFT	AFTED TEST					
.	BEFORE 3	FEST	AFTER TEST	Describes				
	BEFORE 1		AFTER TEST Journal	Bearing				
1	ournal	FEST		Bearing				
1	ournal	Bearing		Bearing				
1	ournal	Bearing		Bearing				
1	ournal	Bearing		Bearing				
1	ournal	Bearing	Journal	Bearing				
1 2 3 4 Build-Up	Engine Measu	Bearing	Journal					
l 2 3 4 Build-Up Camshaft	Engine Measu	Bearing grement Specifications (incl	Journal hes)	825				

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TEST 1	NO.
--------	-----

6V-53T 240-HOUR CHECKLIST

Initials

Task

Fill out page 1 of Before Test and After Test Data Sheets.

Measure and record ring end gap and side clearance.

Measure and record cylinder liner inside diameter (installed).

Measure and record piston-cylinder liner clearance.

Measure and record piston pin-piston bushing clearance and piston pin-rod bushing clearance.

Measure and record block bore diameter.

Measure and record valve depth.

Check valve clearances and replace valves and guides out of specification. Replace valves after three runs.

Measure and record connecting rod bearing shell and bearing journal diameters and clearances.

For major rebuilds only - measure and record oil pump clearances, crankshaft thrust washer thickness and crankshaft end play.

For major rebuilds only - measure and record main bearing shell and bearing journal diameters and clearances.

For major rebuilds only - measure and record camshaft bearing shell and bearing journal diameters.

Calibrate tachometer.

Calibrate flowmeter.

Calibrate load system.

Calibrate temperature indicators.

Calibrate pressure indicators.

Fill engine with reference oil.

Break in engine.

Adjust governor, injector timing, and valve clearance.

Run and record initial power calibration check.

Run shake down.

Run final power calibration check.

Perform airbox inspection.

Drain oil and add five gallon flush oil.

Run flush cycle - 30 minutes at 1200 rpm and 30 #FT.

Drain oil.

planes and the control of the contro

Perform airbox inspection.

Weigh new filter, blowby canisters and intial fill.

Run full load performance determination.

Run test cycle, weigh samples and adds.

Perform after-test full load performance determination.

Drain and weigh oil, filter, and blowby cans.

Measure and record cylinder liner inside diameter.

Disassemble engine stamping liners and pistons.

Measure and record piston pin to piston bushing clearance and piston pin to rod bushing clearance.

Measure and record connecting rod, bearing shell, and bearing rod journal clearances.

Major rebuild only - measure and record main bearing shell and bearing journal diameters and clearances.

Major rebuild only - measure and record camshaft bearing shell and bearing journal diameters.

Rate engine for deposits.

Measure and record ring end gap.

Photograph engine parts.

A-31

6V53T 240-HOUR ENDURANCE TEST LUBRICANT CONSUMPTION RECORD

Fuel Lubricant				Q[]	111	
Test No.		+ + 11	+ + #	0-120 hr 120-240		
ate Started ate Finished	Approximate Consumption (1b)	Weight of Initial Fill Weight of 120-hour Fill Total Weight of Additions Total Weight of Oil Added	Weight of 120-hour Drain Neight of Final Drain Total Weight of Samples Total Weight of Oil Removed	Weight of Used Oil Filter Weight of New Oil Filter Weight of Oil in Filter Total Weight of Oil in Filters	After Test Blowby Can Weight Before Test Blowby Can Weight Total Weight of Oil in Blowby	Total Weight of Oil Added Total Weight of Oil Removed Total Weight of Oil in Filters Total Weight of Oil in Blowby

STATE ESSENTED THE STATE OF THE

フルバルバー

* <u>During</u> test, average oil consumpti 110 consumption is approximated by Total Oil Consumed* Total Lubricant Consumed (= Oil Consumed) Oil Sampled Oil Added Lubricant 0V551 24U-HUUK ENKUKANCE LESI LUBRICANT CONSUMPTION RECORD (DOES NOT INCLUDE INITIAL AND 120 HOUR FILLS) Fuel Sample+ Change(1b) Bottle (= Oil Sample) Lubricant Samples Bottle Wt(1b) Bottle Wt (1b) Test No. Change (1b) Added) (= 0il Lubricant Additions After Add(1b) Before Add (1b) Technician Date Finished Date Started lour 80 120 240 B A-33

APPENDIX F

RATING SHEETS

CRC DIESEL RATING SYSTEM

•				ZE.%	20	UNDER	CROWN	AREA'S DEWE				1	, 	NOT	,	SED	<u> </u>								
			NO. 1 GROOVE, VOLUME.%		PISTON WTD. RATING		NO. 4	AREA'S DEMERIT AREA'S DENE																	
	PISTON NO.	•		NO. 1 GRO	PISTON	SO	NO. 3																		
	N HALING	}	1			LANDS	NO. 2	REA-% DEMERIT AL																	
Orbital and a re-	RATERDATE						NO. 1	REA-% DEMERITA																	
THE MOLTATION	O STATION SHE	I NUMBER	ENGINE NO.				NO. 4	IREA-% DEMERIT" A																	
	3	RY TE	IND NOE			OVES	NO. 3	REA-% DEMERIT A																	
27.01	RATER	LABOF	טואוס.	ruel.		GROOV	NO. 2	AREA-% DEMERIT AREA-% DEMERIT AREA-% DEMERIT AREA-% DEMERIT AREA-% DEMERITAREA-% DEMERIT AREA-% DEMERIT																	
		2	1 1				NO. 1	AREA-% DEMERIT																-	
	TEST PROCEDURE	TEST HOURS	בייאר דייאל	1	#	,	FACTOR		8.	0.75	0.50	0.25	0.15	CARBON	0.100	DB1L 0.075	0.050	0.025	0.010	0.001	LACOUER HATING	0	ZONAL RATING	LOCATION FACTOR	WEIGHTED RATING
	TESTPR	TEST HOURS	יבט בער בטוניי	LUBRICANI		-	I YPE	: : :	Ť		WC ON	38.4 2	כי גרנ	ع ن	81	DBrL	R AL	CAL	۵۸ کا	ا کر	5*	CLEAN	ZOWAL	LOCATIO	WEIGHTE
														A-3	15										

energy by the properties of th

*WEIGHTED TOTAL DEPOSITS

DETROIT DIESEL 6V-33 TEVALUATION

Rating of Engine Deposits and Parts Condition

Oil	-	Test Number	-
Formula	-	Date Test Completed	-
Viscosity Grade	-	Engine Number	-
Fuel	-	Test Stand Number	-
		Hours Completed	-

I. Cylinder Liners

a. Intake Ports

INTAKE PORT PLUGGING

Cylinder No.	Percent Intake Port Restriction
۱L	
2L	
3L	
1 R	
2R	
3 R	
Averag e	-

b. Liner Scuffing

CYLINDER LINER SCUFFING Percent of Total Ring Travel Area Scuffed

Cylinder	Perc	ent Scuff ed	% Total	%	%		
No.	Thrust	Anti-Thrust	Area Scuffed	Glazed	Lacquer		
11,							
2L							
3L							
) R			AND STATE OF THE S				
2 R							
3 R							
Average							
,,,c,ege							

DETROIT DIESEL 6V-53T EVALUATION

Rating of Engine Deposits and Parts Condition

II. Pistons

Cylinder No.	No. l Fire Ring	No. 2	No. 3	No. 4	
1L 2L					

1L			
2L		 	
3L		 	
		 	
1R		 	
2R			Overall
3R		 	 Averag e
Averag e			

^{*} Numbers denote % area ringface burn

b. Piston Ring Groove Carbon, % Filling

Condition of Rings in Grooves

Cylinder No.	No. l Fire Ring	No. 2	No. 3	No. 4
1L				
2L			 	
3L				
1R				, ——
=	····			
2R				
3R			. –	

c. Piston Skirt Rating (Demerit)

Cylinder No.	Thrust	Anti-Thrust
1L		
2L		
3L		
1R		
2R		
3R		
J-1		

d. Oil Control Ring Grooves (Demerit)

Cylinder No.	Upper	Lower
1L		
2L		
3L		
1R		
2R		
3R		

DETROIT DIESEL 6V-53T EVALUATION

Rating of Engine Deposits and Parts Condition

	e.	Oil Drain Holes (pistons)	
	f.	Land Deposits	<u>-</u>
ı. V.		xhaust Valvesombustion Chambers - with exhaust	
••			
٧.	* <u>E</u> :	xhaust Ports	•
ı.	Va	alve Cover, Cylinder Head Decks,	and Oil Pan
	Co	overs	

^{*} Texture in terms of Hard-Medium-Soft Carbon; Depths of A-B-C.

RING STICKING

A CANTONIA PROCESSA POSTOS POPOSOS SESPONOS A CASARA POSTOS A CASARA PORTA POR

	_							
				38				
	Date	Observer		2R				
				18				
Test No.			Piston Number	31				
-	Serial No.	Lubricant		2L				
			:	11				
	Engine Model	Fuel		Ring No.		2	3	4

Indicate by letter — Free or Sluggish, or by number and letter — percent Pinched (cold stuck) or percent Hot stuck (Pages 6 and 7 of Manual).

PISTON GROOVE INSIDE DIAMETER—% RING SUPPORTING CARBON

Test No.

Date	Observer
Serial No.	Lubricant
ingine Model	lau .

	Piston Ring Quadrant	1	2	3	4	1	2	3	4
	11								
	2L								
Piston	3.								
Piston Number	1R								
	2R								
	38								

1 Thrust Side



2 Rear

3 Anti-Thrust Side

Sees A processed in the second interesting in the second i

VALVE DEPOSITS

	Date
lest No.	Serial No.
	Engine Model

Lubricant

Fuel

Observer_

Output Nimbor	1L 2L 3L 1R 2R	INT CARB LACO CARB LACO CARB LACO CARB LACO CARB	ЕХН	TNI	ЕХН	TNI	Lulipi	INT	ЕХН
	38	CARB.							
		LACO							-

*Carbon and Ash: Use Volume Factor Technique (Pages 5 and 40 through 47 of CRC Manual No. 5). †Use Chart, Page 21—indicate H, M, or S (Page 5). Lacquer: Pages 4, 36, and 37.

SECRETAL RECORDS DESCRIBIO DESCRIBIL DESCRIBIO DESCRIBIO DESCRIBIO DE SECRETAL DESCRIBIO DE LA CONTRADA DE SECRETAL DESCRIBIO DE SECRETAL DESCRIBIO DE SECRETAL DE SECRETAL DE SECRETA DE S

EXHAUST VALVE SURFACE CONDITIONS

Engine Model		Test No.			Oate	
		Serial No.			Š	
Fuel		Lubricant			Observer	ver
	11	2L	3L	1R		2R
Freeness in Guide						
Неаd						
Face						
Seat						
Stem						
Тір						

See Pages 1, 2, 16 through 23, and 54 through 65 of CRC Manual No. 5.

TAPPETS, CAMS, AND ROCKER ARMS

Test No.

Date	Observer
Serial No.	Lubricant
Engine Model	Fuel

					Cylinder Number	umber		
			11	21	3L	18	2R	3R
H		INT						
iappet Deposit		ЕХН						
		ſNI						
Tappet Surface Condition	tion	INT						
		ЕХН						
Cam Lobes	ropes							
		TNI						
1	Tip	ЕХН						
	0.1	INT						
Rocker Arms	huilena 1	ЕХН						
	3	INT						
	Shart	ЕХН	ii.					

Lacquer: Pages 4, 36 and 37 of CRC Manual No. 5 See Pages 1, 2, 16 through 23, and 54 through 65.

SURFACE CONDITION

	Date	Observer
Test No.	Serial No.	Lubricant
	Engine Model	Fuel

- 5			·	,	
м					
4		,			
മ					
9					
7					

Note surface condition. See pages 1, 2, 16 through 23 and 54 through 65 of Manual.

PODDA DECOCOR NESSECTO TEXTOS ASSESSED NOTODON NESSECTO ESPERANT ENTROPONA PERSONAL DE SECTIONA DE SECTIONA (CO

APPENDIX G

LUBRICANT ANALYSIS

	:	;						Test	Hour					
	lest Method	New Oil	2	9	3	8	801	120 140	140	160	180	00Z	220	240
Viscosity at 40°C	0 445	×			×			×			×			•
Viscosity at 100°C	D 445	×			×			×			: ×			< >
TAN	799 a	×			×			×			: ×			< >
TBN	799 a	×			×			×			: ×			< >
Pentane B											ł			4
Insolubles	D 893	×			×			×			×			,
Toluene B											.			∢
Insolubles	D 893	×			×			×			×			
Flash Point	D 92	×									ŧ			< >
Fuel Dilution	D 3524		×					×						< >
Te.	đ	×	×	×	×	×	×	×	×	×	×	×	×	٠ 🛏
ಪ	•	×	×	×	×	×	×	×	×	×	×	: ×	: H	۰ >
Pb	•	×	×	×	×	×	×	×	×	×	×	: ×	£ 34	<
رد رد	•	×	×	×	×	×	×	×	×	×	×	: ×	: ×	٠ 🛏
¥!	•	×	×	×	×	×	×	×	×	×	×	: ×	: ×	· ×

a " by any of the following mathods: AA, XRF, emission spec.

HON KRING HONEY BOOME KRING HASSEN FOR THE STANK REPORT HOSSEN FOR THE FOREST FOR THE PARTY OF THE

APPENDIX H 6V-53T TEST NO.: LUBRICANT:

WEAR MEASUREMENTS

Cylinder Liner Bore Diameter Change*

	5, 2		
	- 1L T-AT** F-B	Cylinder Number 2L T-AT F-B	3L T-AT F-B
Top Middle Bottom			
_	1R <u>T-AT</u> <u>F-B</u>	Cylinder Number 2R T-AT F-B	3R <u>T-AT</u> <u>F-B</u>
Top Middle Bottom			
		Average Change	

T-AT F-B

Top Middle F-P

Bottom
Overall Average Change:

Piston Ring End Gap Change

Ring Number	<u>1L</u>	<u>2L</u>	<u>3L</u>	<u>1R</u>	<u>2R</u>	<u>3R</u>	Average Change
1 2							
3							
4							
5							
6							
7							

Overall Average Change:

- * All dimensions given are in inches and (millimeters).
- ** T-AT= Thrust -Anti-thrust Direction, F-B= Front-Back Direction

APPENDIX B

ENGINE-LUBRICANT COMPATIBILITY TEST 240-HOUR TRACKED-VEHICLE CYCLE USING 6V-53T DIESEL FUEL

Lubricant AL-12271-L, Test No. 31

ENGINE-LUBRICANT COMPATIBILITY TEST 240-HOUR TRACKED-VEHICLE CYCLE USING 6V-53T DIESEL ENGINE

Test Lubricant: AL-12271-L Test Fuel: Caterpillar 1-H Engine Test Number: 31 Date Completed: 28 June 1983

Conducted For

U.S. Army Mobility Equipment Research and Development Command Materials, Fuels and Lubricants Fort Belvoir, Virginia

by

U.S. Army Fuels and Lubricants Research Laboratory Southwest Research Institute San Antonio, Texas 78284

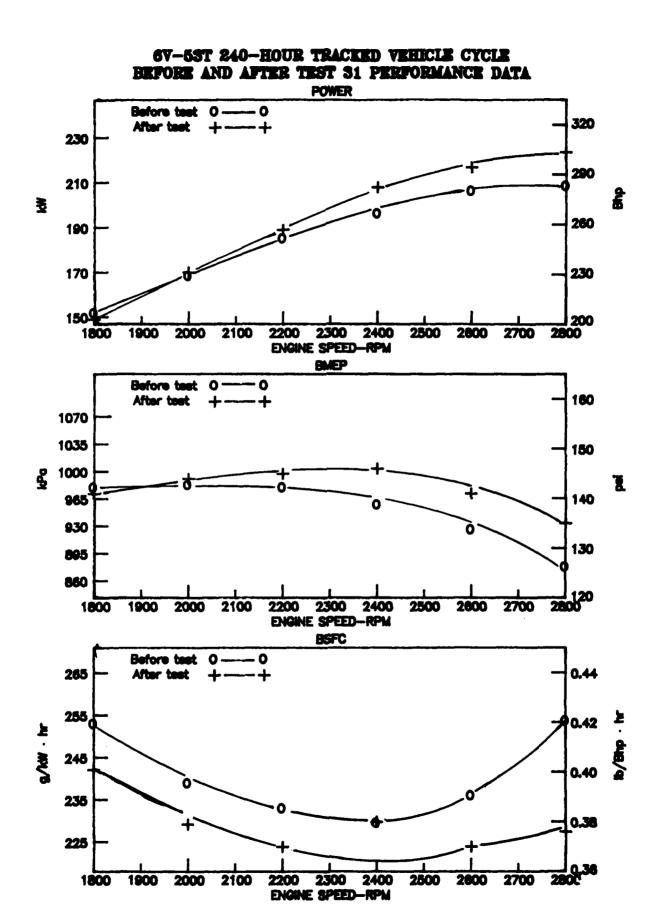
6V-53T TEST 31

ENGINE REBUILD MEASUREMENTS*

Model Number: 5063-5395 Serial Number: 6D-157211

	<u>Min</u>	Max	Avg	Spec	ified Limits
Cylinder Block Bore					
Inside Diameter (Bottom)	4.3566(110.658)	4.3582(110.698)	4.3573(110.675)	4.3565(110.655)	- 4.3575(110.681) New - 4.3595(110.731) Max
Out-of-Round Taper	0.0000 0.0000	0.0010(0.025) 0.0004(0.010)	0.0004(0.010) 0.0002(0.005)		- 0.0015 (0.038) Max - 0.0015 (0.038) Max
Cylinder Liners (Installed)					
Inside Diameter	3.8754(98.435)	3.8765(98.463)	3.8761 (98.453)	3.8752(98.430)	- 3.8767(98.468)
Out-of-Round	0.0000	0.0011(0.028)	0.0003(0.0077)		- 0.0015(0.038) Max
Taper	0.0001(0.003)	0.0006(0.015)	0.0003(0.0077)		- 0.0015(0.038) Max
Piston Diameter					
(at skirt)	3.8678(98.242)	3.8690(98.273)	3.8683 (98.255)	3.8669(98.219)	- 3.8691 (98.275)
Piston Skirt to Cylinder					
Liner Clearance	0.0069(0.175)	0.0086(0.218)	0.0077(0.196)	0.0061(0.155)	- 0.0098(0.249)
Compression Rings					
Gap (No. 1, Fire Ring)	0.030(0.76)	0.036(0.91)	0.034(0.86)	0.020(0.51)	- 0.046(1.17)
Gap (Nos. 2, 3, 4)	0.029(0.74)	0.036(0.91)	0.034(0.86)	0.020(0.51)	- 0.036(0.91)
Ring-to-Groove Clearance					
Top (No. 1, Fire Ring)	0.004(0.10)	0.004(0.10)	0.004(0.10)	0.003(0.08)	- 0.006(0.15)
No. 2, Compression Ring	0.008(0.20)	0.008(0.20)	0.008(0.20)	0.007(0.18)	- 0.010(0.25)
No. 3 and 4, Compression Rings	0.006(0.15)	0.006(0.15)	0.006(0.15)	0.005(0.13)	- 0.008(0.20)
	,		,	***************************************	01000(0120)
Oil Control Rings,					
<u>Nos. 5, 6, 7</u> Gap	0.015(0.38)	0.020(0.51)	0.017(0.43)	0.010(0.25)	- 0.025(0.64)
Ring-to-Groove Clearance	0.003(0.08)	0.004(0.10)	0.004(0.10)	0.0015(0.038)	- 0.0055(0.140)
J		, ,	• •		
Piston Pin Pin-to-Piston Bushing					
Clearance	0.0026(0.066)	0.0030(0.076)	0.0030(0.076)	0.0025(0.064)	- 0.0034(0.086)
Pin-to-Connecting Rod	,	,	.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	***************************************	
Bushing Clearance	0.0016(0.041)	0.0017(0.043)	0.0017(0.043)	0.0010(0.025)	- 0.0019(0.048)
Connecting Rod Bearing-					
to-Journal Clearance	0.0024(0.061)	0.0028(0.071)	0.0026(0.067)	0.0011(0.028)	- 0.0041(0.104)
Main Bearing-to-Journal					
Clearance	0.0039(0.099)	0.0040(0.102)	0.0039(0.099)	0.0010(0.025)	- 0.0040(0.102)
Camshaft Bearing-to-Shaft					
Clearance	0.0055(0.140)	0.0059(0.150)	0.0057(0.145)	0.0045(0.114)	- 0.0060(0.152)
	,,				

^{*}Measurements are in inches and (mm)



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6V-53T 240-HOUR TRACKED VEHICLE ENDURANCE TEST TEST 31 OPERATING CONDITIONS SUMMARY

Lubricant: AL-12271-L Fuel: Caterpillar 1-H

	Maximum Pow (2800 R		Maximum Tor (2200 F	
	- 	Standard		Standard
	<u>Mean</u>	Deviation	Mean	Deviation
Engine Speed, rpm	2802	3.05	2204	3.97
Torque, ft-lb (N-m)	517 (701)	3.8(5.1)	580 (786)	3.01(4.1)
Fuel Consumption, 1b/hr(kg/hr)	104.6(47.4)	0.94(0.42)	88.96 (40.35)	0.67(0.30
Observed Power, Bhp(kW)	275.3(205.6)	2.09(1.56)	242.7(181.3)	1.43(1.07)
BSFC, 1b/Bhp-hr(g/kW-hr)	0.380(230.79)	0.004(2.31)	0.367(222.6)	0.002(1.39)
Temperatures, °F(°C)				
Exhaust before Turbo	905 (485)	30.10(16.7)	901 (483)	26.4(14.7)
Exhaust after Turbo	731 (389)	94.20(52.3)	775 (413)	50.4(27.99)
Water Jacket Inlet	157(69)	1.99(1.1)	156(69)	1.24(0.69)
Water Jacket Outlet	170 (76)	1.95(1.1)	170 (76)	1.20(0.67)
Oil Sump	224(106)	1.76(1.0)	218(103)	1.59(0.88)
Fuel at Filter	95 (35)	2.50(1.4)	92(33)	2.06(1.15)
Inlet Air	94 (35)	5.30(2.9)	92(34)	4.33(2.41)
Airbox	263(128)	4.55(2.5)	221(105)	3.42(1.90)
Pressures				
Exhaust before Turbo,				
psi(kPa)	11.90(81.93)	0.76(5.27)	7.76(53.50)	0.28(1.93)
Exhaust after Turbo,				
in. Hg(kPa)	2.95(9.94)	0.17(0.57)	1.88(6.35)	0.08(0.25)
Compressor Discharge, psi(kPa)	12.23(84.30)	0.50(3.43)	8.69(59.95)	0.21(1.45)
Blower Discharge, psi(kPa)	17.68(121.93)	0.69(4.73)	10.53(72.58)	0.24(1.62)
Oil Gallery, psi (kPa)	54.11(373.09)	0.70(4.85)	47.25 (325.76)	0.93(6.42)
Intake Vacuum, in. H ₂ O(kPa)	8.30(2.07)	0.33(0.08)	5.03(1.25)	0.28(0.07)
Ambient Conditions				
Dry Bulb Temperature, °F(°C)	81.2(27.3)	5.64(3.13)	80.1(26.7)	5.07(2.82)
Wet Bulb Temperature, °F(°C)	75.7(24.3)	6.73(3.02)	74.5(23.6)	6.05(3.36)
Barometric Pressure,				
in. Hg(kPa)				
(Both modes of operation)	29.2(98.6)	0.26(0.88)		

^{*68%} of the values for a given variable occur within ±1 standard deviation of the mean; 95% occur within ±2 standard deviations.

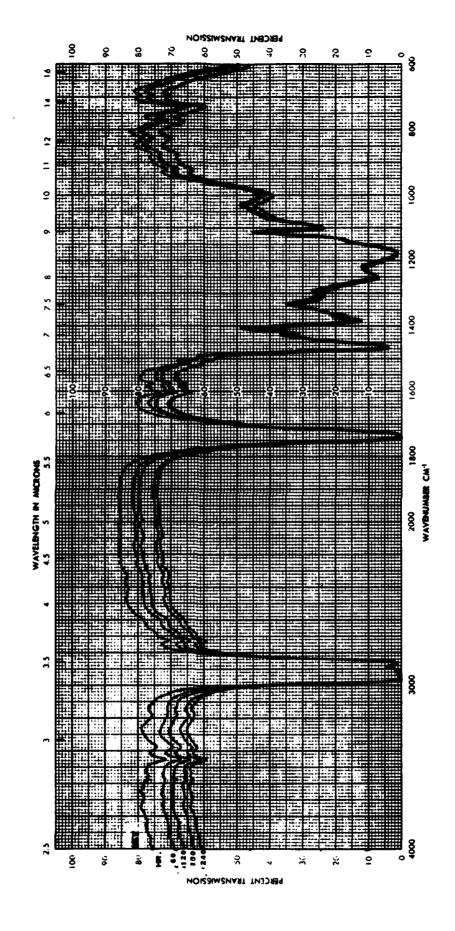
6V-53T TEST 31 LUBRICANT ANALYSIS Lubricant: AL-12271-L

	ASTM						Test	Test Time. Hours	ure					
	Me thod	9	20	07	09	80	100	22	140	160	<u>8</u>	200	220	240
Kinematic viscosity @ 40°C (104°F) cSt	D445	27.81	ı	l	28.97	ļ	;	28.78	1	i	27.68	i	1	26.55
Kinematic viscosity @ 100°C (212°F) cSt	D445	6.19	6.95	6.47	6.32	6.33	6.39	6.42	6.17	6.24	6.13	6.11	5.96	90.9
Total Acid Number mg KOH/8	D664	0.20	1	1	0.31	t	‡	0.23	ı	ł	0.23	ı	1	0.23
Total Base Number mg KOH/8	D664	6.95	i	ı	5.21	ł	ı	3.83	1	ĺ	4.85	ł	1	3.12
Pentane B Insolubles	D893	0.01	ı	1	0.04	ı	ı	0.18	1	ŀ	0.11	ı	ı	0.21
Toluene B Insolubles	D693	0.01	ı	ŀ	0.0	i	1	0.17	ı	ı	0.11	1	1	0.19
Flash Point, °C	D92	244	ı	ŀ	1	ı	ı	244	ł	i	i	i	1	229

INFRARED SPECTRUM 6V-53T TEST 31

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Lubricant: AL-12271-L



6V-53T TEST 31 Lubricant: AL-12271-L

TOTAL CONSUMPTION AND WEAR METALS BY XRF

m m.			Wear Me	tals,ppm
Test Time, Hours	Total Oil Con	sumed, 1b(kg)	Fe	Cu
0			11	<40
20	10.07	(4.57)	27	19
40	20.65	(9.37)	22	22
60	30.37	(13.78)	26	20
. 80	37.77	(17.13)	26	15
100	45.13	(20.47)	28	35
120	011 chan	ge	26	<10
140	53.21	(24.13)	15	<10
160	60.60	(27.49)	14	<10
180	69.49	(31.52)	23	<10
200	76.60	(34.75)	23	<10
220	83.41	(37.83)	18	<10
240	94.62	(42.92)	20	<10

Average oil consumption rate: 0.39 lb/hr (0.18 kg/hr)

6V-53T TEST 31 Lubricant: AL-12271-L

WEAR MEASUREMENTS*

Cylinder Liner Bore Diameter Change

	17		<u>Cylinder</u> 21.	Number	21			
	T-ATAA	7-3	T-AT	<u>P-B</u>	<u>T-AT</u>	<u>F-B</u>		
Top Middle Bottom	+0.0006(0.015) -0.0001(-0.003) -0.0005(-0.013)	-0.0007(-0.018) -0.0005(-0.013) -0.0003(-0.008)	+0.0006(0.015) 0.0000 -0.0003(-0.008)	-0.0006(-0.015) -0.0003(-0.008) -0.0002(-0.005)	+0.0003(0.008) -0.0002(-0.005) -0.0003(-0.008)	-0.0007(-0.018) -0.0002(-0.005) -0.0001(-0.003)		
Cylinder Number 2R 3R								
	T-AT*	<u> F-B</u>	T-AT	<u> </u>	T-AT	F-B		
Top Middle Bottom	+0.0004(0.010) 0.0000 -0.0003(-0.008)	-0.0004(-0.010) -0.0001(-0.003) 0.0000	+0.0004(0.010) +0.0003(0.008) 0.0000	-0.0001(-0.003) -0.0001(-0.003) -0.0003(0.008)	+0.0004(0.010) +0.0001(0.003) -0.0001(-0.003)	-0.0003(-0.008) -0.0003(-0.008) -0.0001(-0.003)		
			Average	Change				

T-AT F-B +0.0005(0.013) 0.0000 -0.0003(-0.008) -0.0005(-0.013) -0.0003(-0.008) -0.0002(-0.005) Top Middle Bottom

Overall average change: -0.0001(-0.003)

Piston Ring End Gap Change

Ring Number	<u>1L</u>	<u>2L</u>	<u>3L</u>	<u>1R</u>	<u>2R</u>	<u>3R</u>	Average Change
1	+0.002(0.05)	+0.004(0.10)	+0.002(0.05)	+0.002(0.05)	+0.008(0.20)	+0.002(0.05)	+0.003(0.08)
2	0.000	+0.002(0.05)	+0.001(0.03)	+0.004(0.10)	+0.002(0.05)	+0.002(0.05)	+0.002(0.05)
3	+0.001(0.03)	+0.001(0.03)	+0.001(0.03)	+0.002(0.05)	+0.002(0.05)	+0.003(0.08)	+0.002(0.05)
4	0.000	+0.001(0.03)	+0.002(0.05)	+0.002(0.05)	+0.003(0.08)	+0.002(0.05)	+0.002(0.05)
5	+0.007(0.18)	+0.007(0.18)	+0.007(0.18)	+0.007(0.18)	+0.006(0.15)	+0.007(0.18)	+0.007(0.18)
6	+0.009(0.23)	+0.006(0.15)	+0.006(0.15)	+0.006(0.15)	+0.005(0.13)	+0.006(0.15)	+0.006(0.15)
7	+0.008(0.13)	+0.006(0.15)	+0.006(0.15)	+0.004(0.10)	+0.004(0.10)	+0.007(0.18)	+0.006(0.15)

Overall average change: +0.004(0.10)

^{*}All dimensions are given in inches (mm).
**T-AT = Thrust-Antithrust Direction; F-E = Front-Back Direction.

6V-53T TEST 31

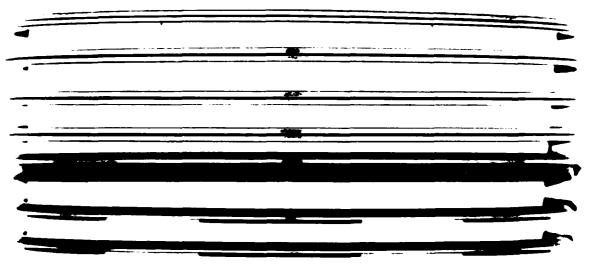
Lubricant: AL-12271-L

POST TEST ENGINE CONDITION AND DEPOSITS

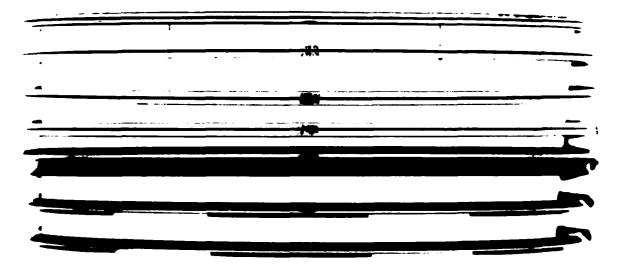
A. Cylinder Liner	11	2 1 .	3L	1R	2R	3R	Average
Intake Port Plugging,							averege.
% restriction	<1	<1	<1	<1	<1	<1	<1
Liner Scuffing,							
% Area							
Thrust	0	3	2	1	7	4	2.83
Anti-Thrust	2	6	4	9 5	2	2	4.17
% Total Area Scuffing	1	4.5	3	,	4.5	3 OVERALL:	3.50 3.50
% Area Bore Polished	3	1	1	3	•	2	1 00
Thrust Anti-Thrust	5	i	2	1	2 1	3	2.00 2.17
Z Avg. Area Bore	•	-	_	•	•	•	••••
Polished	4	1	1.5	2	1.5	2.5	2.08
			•			OVERALL:	2.08
B. Pistons							
Ring Face Distress, (demerits)							
No. 1	10.50	15.25	4.50	5.50	12.00	5.00	8.79
No. 2	0.25	1.25	0.75	0.00	8.75	0.50	1.92
No. 3	0.50	0.50	3.25	0.50	21.25	0.00	4.33
No. 4	0.25	0.50	1.25	0.00	18.75	0.25	3.50
						OVERALL:	3.13
Piston Skirt Rating							
Thrust	LS*	5%SC	S	S	S	S	
Anti-Thrust	S	LS	S	5 XS C	S	S	
Piston WTD Rating**	266.38	298.50	279.50	259.00	278.63	279.00	276.84
Ring Sticking							
No. 1	F	F	F	P	F	<u>P</u>	
No. 2	F,C***	F	F,C F	F	ŗ	r	
No. 3 No. 4	F F	P P	F	F F	F F	F	
	•	•	•	-	•	•	
C. Exhaust Valves							
Deposits							
Head	-		_	· ——		→	
Face Tulip			\AHC \AHC.			-	
Stem	-		49 Lac	drez++ —		-	
Surface Condition							
Freeness in Guide	F	r	•	F	7	P	
Head	-		Normal			-	
Face	-		Normal-				
Seat Stem	_		Normal Normal				
Tip			Normal			→	
D. Other Ratings							
Homes Odl Comens Barr							
Upper Oil Control Ring Expansion Force,							
lbs.	22.8	22.4	22.2	22.0	21.0	21.0	21.9
Berring Surface Condict	0 0						
Bearing Surface Conditi Main Bearings		Bearing 1	has deep	trooves c	ut down	to copper	
Rod Bearings	R-1 Cont	necting R	od Bearing	worn the		copper fr	ont
-	and rea	er with a	wear in	middle			
Oil Pan	802 hA :	sludge+++					
#L = Light, S = Scratch	es, PM -	Plating	selted. N	- Normal	, sc - s	cuffing, B	- Burn

^{***}AL = Light, S = Scratches, PM = Plating Melted, N = Normal, SC = Scuffing, B = Burn ***CRC Weighted Total Deposits (0 = least, 900 = most)
****AMS = Hotstuck, CS Cold Stuck, P = Pinched, F = Free, N = Normal, C = Chipped
+HC = Hard Carbon; the number-letter, prefix indicates carbon depth with
***kA = least to J = most
++= The higher the number, the darker the lacquer (0 = lightest, 9 = darkest)
+++Sludge depth ratings range from A to J. ***kA equals an average depth which is approximately one half of the "A" depth as illustrated in CRC Manual No. 10.

6V53T(#31) 1-L



6V53T(#31) 1-R



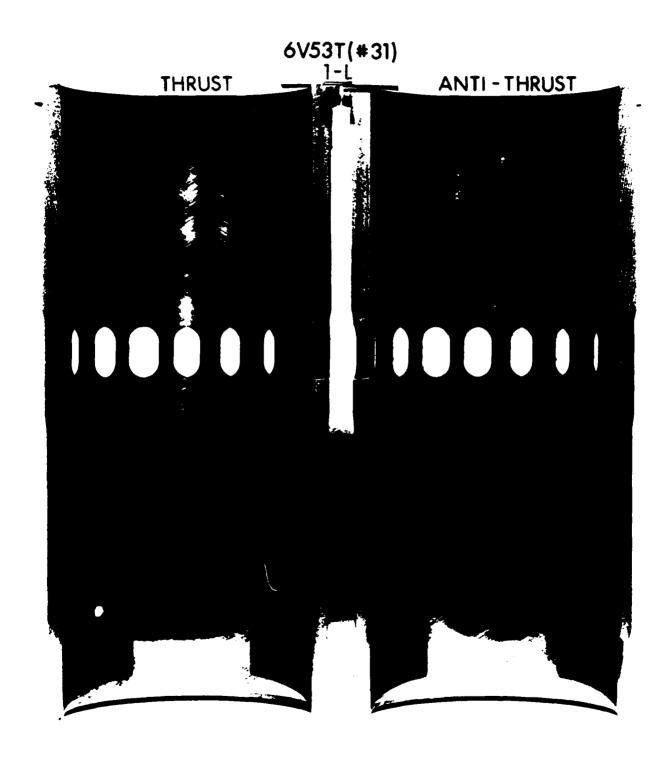


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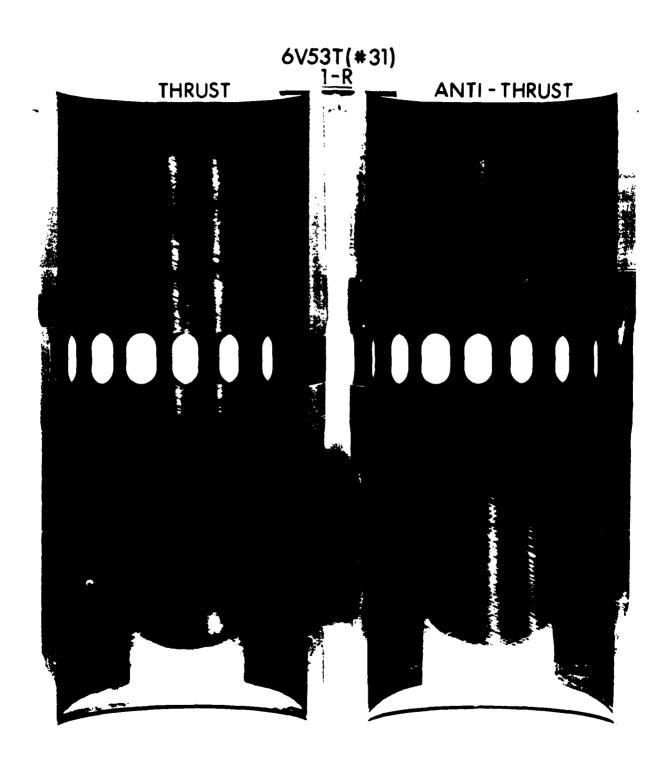


6V53T(#31) 1-R-AT

6V53T(#31) 1-R-T

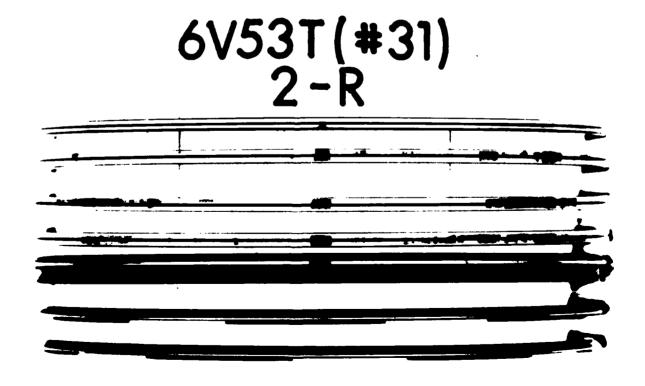


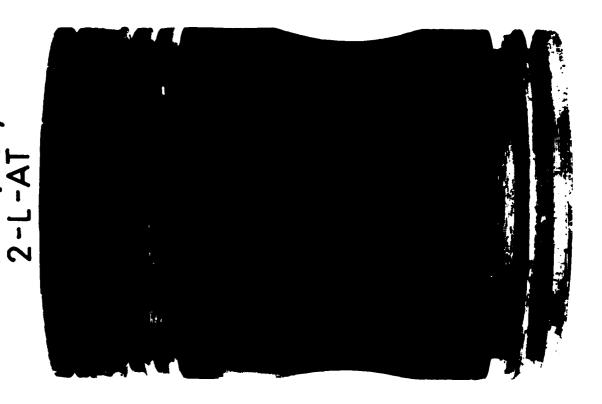
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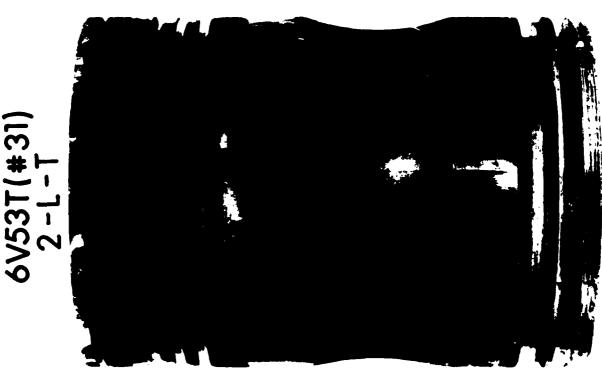




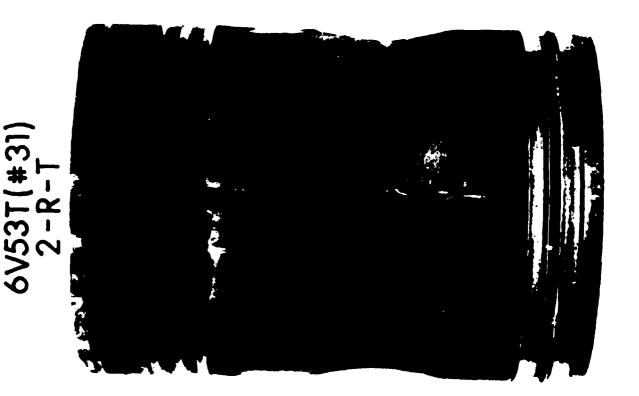


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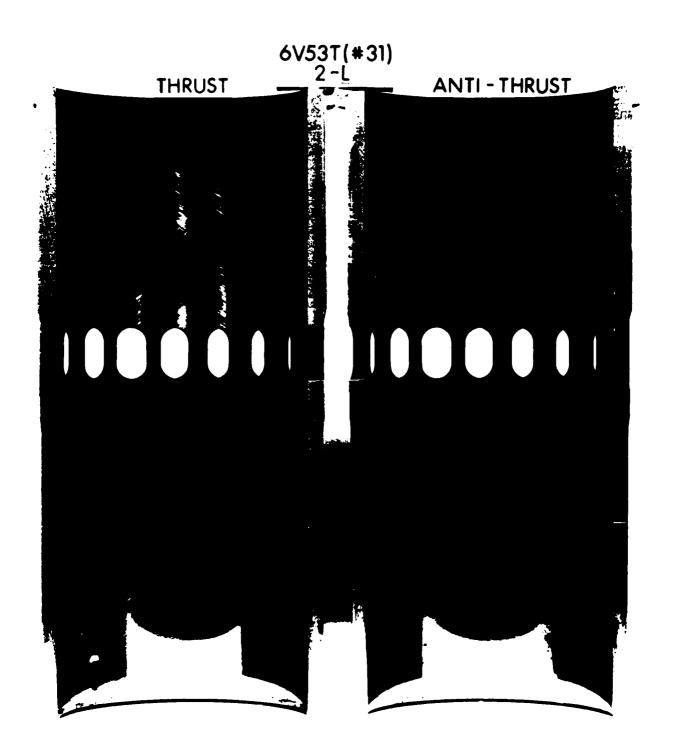
6V53T(#31)



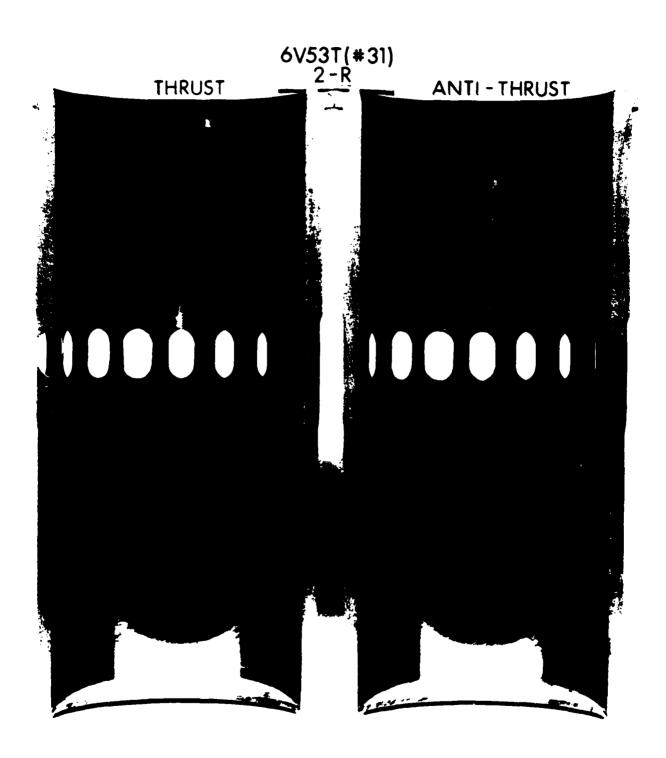
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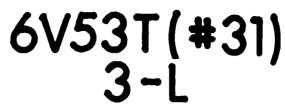
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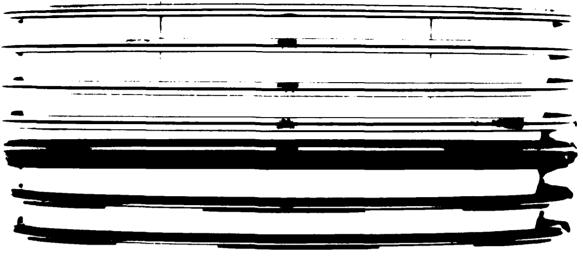


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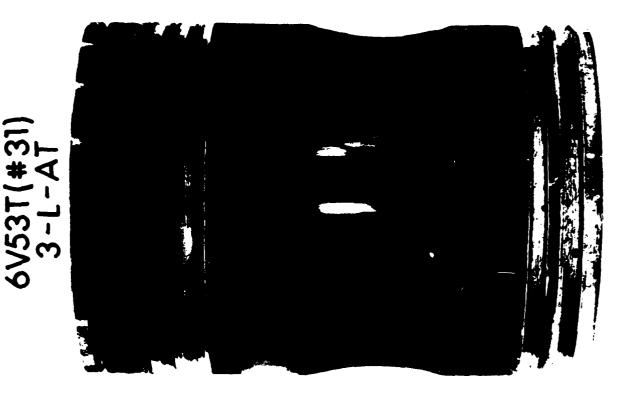
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6V53T(#31) 3-R

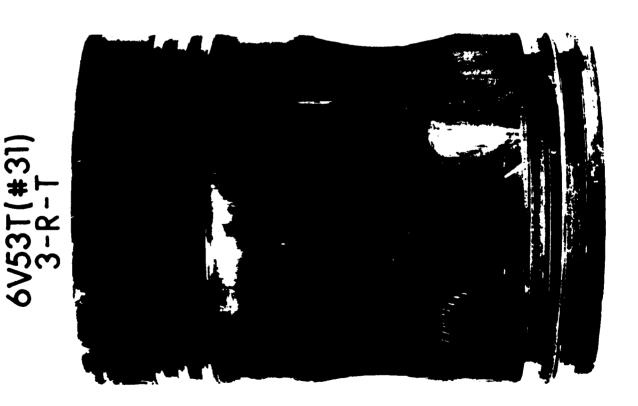




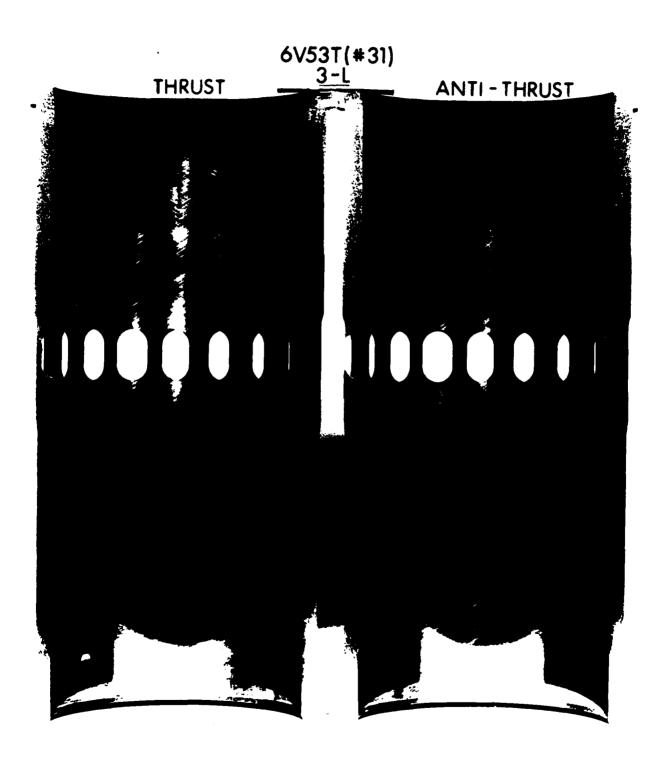
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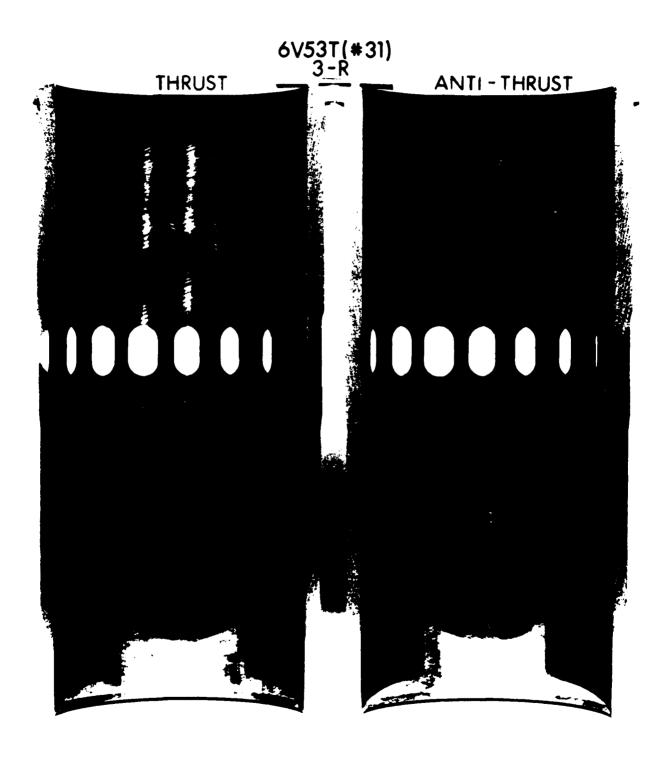
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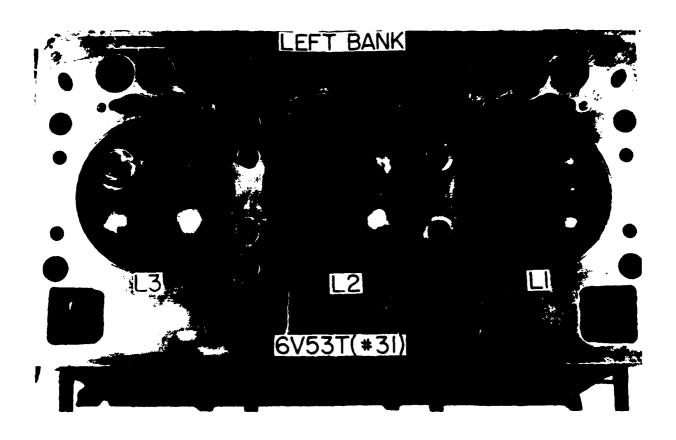


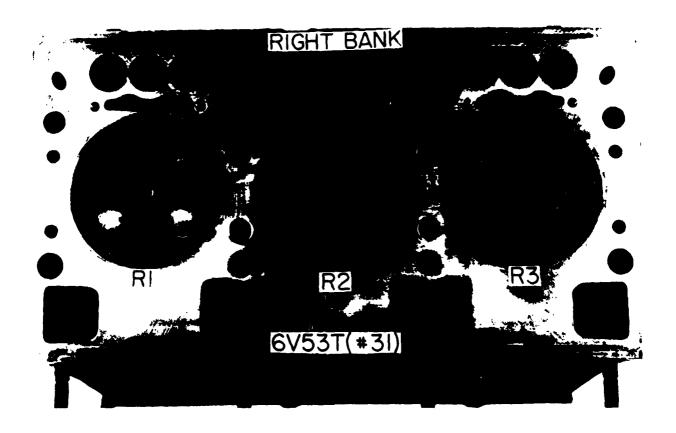
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APPENDIX C

ENGINE-LUBRICANT COMPATIBILITY TEST 240-HOUR TRACKED-VEHICLE CYCLE USING 6V-53T DIESEL FUEL

Lubricant AL-12271-L, Test No. 32

ENGINE-LUBRICANT COMPATIBILITY TEST 240-HOUR TRACKED-VEHICLE CYCLE USING 6V-53T DIESEL ENGINE

Test Lubricant: AL-12272-L Test Fuel: Caterpillar 1-H Engine Test Number: 32* Date Completed: 20 July 1983

Conducted For

U.S. Army Mobility Equipment Research and Development Command Materials, Fuels and Lubricants Fort Belvoir, Virginia

bу

U.S. Army Fuels and Lubricants Research Laboratory Southwest Research Institute San Antonio, Texas 78284

*Test stopped at 60 hours due to severe scuffing and #2 main bearing failure.

6V-53T TEST 32

ENGINE REBUILD MEASUREMENTS*

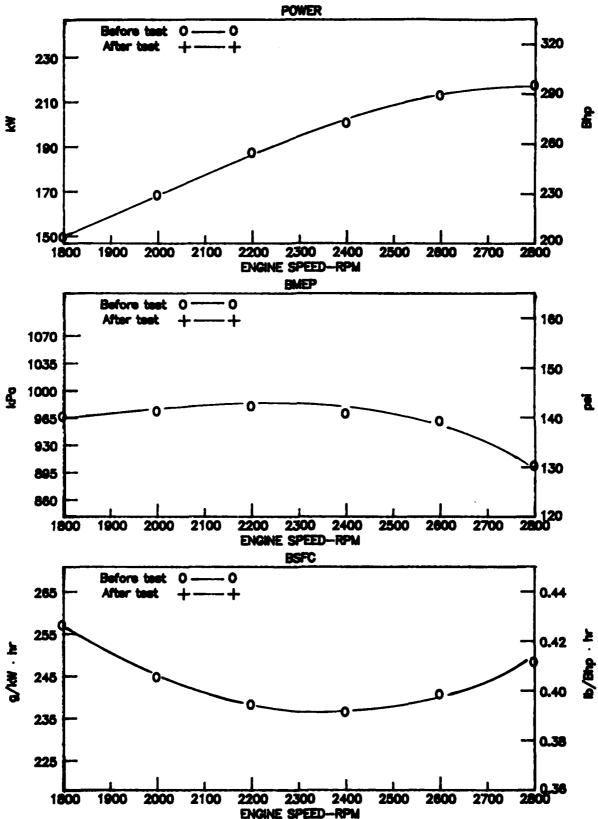
Model Number: 5063-5395 Serial Number: 6D-157211

	<u>Hin</u>	Max	Ave	Specified Limits	
Cylinder Block Bore					
Inside Diameter (Bottom)	4.3565(110.655)	4.3582(110.698)	4.3573(110.675)	4.3565(110.655)	- 4.3575(110.681) New - 4.3595(110.731) Max
Out-of-Round Taper	0.0000 0.0000	0.0012(0.030) 0.0012(0.030)	0.0004(0.010) 0.0004(0.010)		- 0.0015 (0.038) Max - 0.0015 (0.038) Max
Cylinder Liners (Installed)					
Inside Diameter Out-of-Round Taper	3.8756(98.440) 0.0000 0.0000	3.8766(98.466) 0.0005(0.013) 0.0007(0.018)	3.8761 (98.453) 0.0002 (0.005) 0.0002 (0.005)	3.8752(98.430)	- 3.8767(98.468) - 0.0015(0.038) Max - 0.0015(0.038) Max
Piston Diameter (at skirt)	3.8680(98.247)	3.8690(98.273)	3.8685(98.260)	3.8669(98.219)	- 3.8691 (98.775)
Piston Skirt to Cylinder Liner Clearance	0.0069(0.175)	0.0084(0.213)	0.0076(0.193)	0.0061(0.155)	- 0.0098(0.249)
Compression Rings Gap (No. 1, Fire Ring) Gap (Nos. 2, 3, 4)	0.030(0.76) 0.030(0.76)	0.036(0.91) 0.036(0.91)	0.033(0.84) 0.032(0.81)	0.020(0.51) 0.020(0.51)	- 0.046(1.17) - 0.036(0.91)
Ring-to-Groove Clearance Top (No. 1, Fire Ring) No. 2, Compression Ring No. 3 and 4, Compression Rings	0.003(0.08) 0.007(0.18) 0.006(0.15)	0.003(0.08) 0.008(0.20) 0.007(0.18)	0.003(0.08) 0.008(0.20) 0.006(0.15)	0.003(0.08) 0.007(0.18) 0.005(0.13)	- 0.006(0.15) - 0.010(0.25) - 0.008(0.20)
Oil Control Rings,	0.000(0.13)	0,007(0010)	•••••	,	
Gap Ring-to-Groove Clearance	0.017(0.43) 0.002(0.05)	0.019(0.48) 0.003(0.08)	0.018(0.46) 0.003(0.08)	0.010(0.25) 0.0015(0.038)	- 0.025(0.64) - 0.0055(0.140)
Piston Pin Pin-to-Piston Bushing Clearance	0.0032(0.081)	0.0034(0.086)	0.0033(0.084)	0.0025(0.064)	- 0.0034(0.086)
Pin-to-Connecting Rod Bushing Clearance	0.0019(0.048)	0.0019(0.048)	0.0019(0.048)	0.0010(0.025)	- 0.0019(0.048)
Connecting Rod Bearing- to-Journal Clearance	0.0018(0.046)	0.0036(0.091)	0.0028(0.071)	0.0011(0.028)	- 0.0041(0.104)
Main Bearing-to-Journal Clearance	0.0039(0.099)	0.0040(0.102)	0.0039(0.099)	0.0010(0.025)	- 0.0040(0.102)
Camshaft Bearing-to-Journ Clearance	al 0.0055(0.140)	0.0059(0.150)	0.0057(0.145)	0.0045(0.114)	- 0.0060(0.152)

^{*}Measurements are in inches and (mm)

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6V-5ST 240-HOUR TRACKED VEHICLE CYCLE BEFORE TEST 32 PERFORMANCE DATA



6V-53T

240-HOUR TRACKED VEHICLE CYCLE ENDURANCE TEST TEST 32

OPERATING CONDITIONS SUMMARY

Lubricant: AL-12272-L Fuel: Caterpillar 1-H

	Maximum Po (2800		Maximum Torque Mode (2200 RPM)		
	·	Standard		Standard	
	<u>Mean</u>	Deviation	Mean	Deviation	
Engine Speed, rpm	2800	3.11	2200	4.49	
Torque, ft-1b (N-m)	516(700)	4.00(5.41)	580 (786)	2.71(3.67)	
Fuel Consumption, 1b/hr(kg/hr)	111(50.4)	0.67(0.30)	94 (42.4)	0.66(0.30)	
Observed Power, Bhp(kW)	275 (205)	2.12(1.58)	242(181)	1.25(0.94)	
BSFC, 1b/Bhp-hr(g/kW-hr)	0.405(246)	0.003(1.82)	0.386(234)	0.003(1.67)	
Temperatures, °F(°C)					
Exhaust before Turbo	887(475)	25.00(13.9)	877(470)	23.90(13.3)	
Exhaust after Turbo	739(393)	17.50(9.75)	767 (409)	21.80(12.1)	
Water Jacket Inlet	157(69.6)	1.12(0.62)	155(68.6)	1.41(0.78)	
Water Jacket Outlet	170 (76.9)	1.29(0.71)	169(76.0)	1.60(0.89)	
Oil Sump	229(110)	1.63(0.91)	221(105)	2.09(1.16)	
Fuel at Filter	92 (33.4)	1.15(0.64)	90(32)	1.04(0.58)	
Inlet Air	93 (34.0)	2.89(1.61)	91 (32.8)	1.94(1.08)	
Airbox	252(122)	3.83(2.13)	209(98.4)	2.09(1.16)	
Pressures					
Exhaust before Turbo,					
psi(kPa)	12.3(84.9)	0.17(1.17)	8.1(55.7)	0.14(0.98)	
Exhaust after Turbo,					
in. Hg(kPa)	3.1(10.6)	0.22(0.73)	1.9(6.32)	0.22(0.74)	
Compressor Discharge, psi(kPa)	12.9(89.0)	0.37(2.56)	9.0(61.7)	0.30(2.06)	
Blower Discharge, psi(kPa)	19.2(132.0)	0.45(3.10)	11.4(78.9)	0.46(3.20)	
Oil Gallery, psi (kPa)	49.8(344.0)	1.70(11.70)	43.6(300.0)	1.15(7.90)	
Intake Vacuum, in. H ₂ 0(kPa)	8.6(2.14)	0.33(0.08)	5.0(1.24)	0.29(0.07)	
Ambient Conditions					
Dry Bulb Temperature, F(°C)	79.42(26.3)	3.79(2.11)	77.70(25.4)	2.03(1.13)	
Wet Bulb Temperature, °F(°C)	74.76(23.8)	2.34(1.30)	74.40(23.5)	2.43(1.35)	
Barometric Pressure,					
in. Hg(kPa)					
(Both modes of operation)	29.16(98.5)	0.10(0.34)			

^{*68%} of the values for a given variable occur within ±1 standard deviation of the mean; 95% occur within ±2 standard deviations.

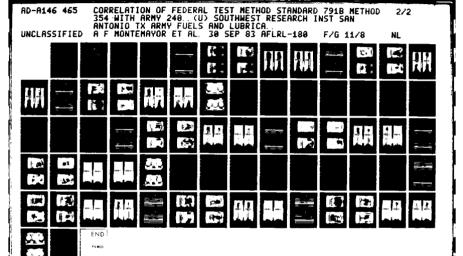
6V-53T
TEST 32
LUBRICANT ANALYSIS
Lubricant: AL-12272-L

	ASTM Test		Test Time	e, Hours	
	Method	0	20	40	60
Kinematic viscosity @ 40°C (104°F) cSt	D445	32			30.6
Kinematic viscosity @ 100°C (212°F) cSt	D445	6.37	5.95	5.92	5.89
Total Acid Number mg KOH/g	D664	2.10			2.41
Total Base Number mg KOH/g	D664	7.91			3.53
Pentane B Insolubles wt%	D893	0.0			0.06
Toluene B Insolubles wt%	D893	0.0			0.06
Flash Point, °C	D92 ·	229			234

TOTAL CONSUMPTION AND WEAR METALS BY XRF

	m 1 0/1 0	1 11 71)		tals,ppm
Test Time, Hours	Total Oil Con	sumed, ID(Kg)	. <u>Fe</u>	<u>Cu</u>
0			20	<10
20	6.16	(2.79)	76	<10
40	16.72	(7.58)	163	<10
60	26.16	(11.87)	205	22

Average oil consumption rate: 0.44 lb/hr (0.20 kg/hr)





MICROCOPY RESOLUTION TEST CHART

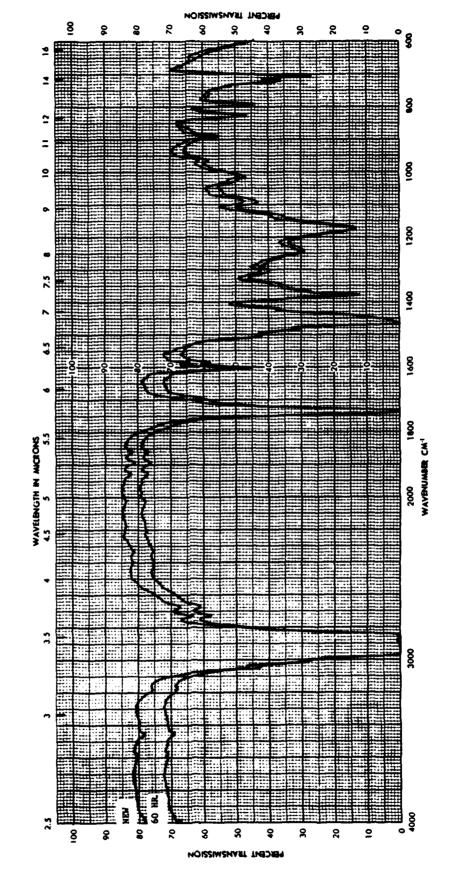
INFRARED SPECTRUM

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6V-53T

TEST 32

Lubricant: AL-12272-L



6V-53T TEST 32

Lubricant: AL-12272-L

WEAR MEASUREMENTS*

Cylinder Liner Bore Diameter Change

			Cylinder	Number							
	T-AT**	P-B	<u>T-AT</u> <u>2L</u>	P-B	<u>T-AT</u>	<u>F-B</u>					
Top Middle Bottom	+0.0001(0.03) 0.0000 -0.0003(-0.008)	-0.0005(-0.013) -0.0005(-0.013) -0.0005(-0.013)	-0.0001(-0.003) -0.0001(-0.003) -0.0004(-0.010)	-0.0005(-0.013) -0.0003(-0.008) -0.0005(-0.013)	+0.0006(0.015) -0.0004(-0.010) -0.0004(-0.010)	-0.005(-0.013) -0.0006(-0.015) -0.0005(-0.013)					
	Cylinder Number 1R 2R 3R										
	T-AT*	F-B	<u>T-AT</u>	<u>F-B</u>	<u>T-AT</u>	F-8					
Top Middle Bottom	+0.0001(0.003) -0.0004(-0.10) -0.0002(-0.005)	-0.0005(-0.013) -0.0006(-0.015) -0.0004(-0.010)	+0.0003(0.008) -0.0001(-0.003) -0.0004(-0.010)	-0.0003(-0.008) +0.0002(0.005) -0.0003(-0.008)	Not Measured - Removed liner an Removed liner an						
			Average	Change							
			T-AT	P_8							

T-AT F-B

+0.0002(0.005) -0.0002(-0.005) -0.0003(-0.008) -0.0005(-0.013) -0.0004(-0.010) -0.0004(-0.010) Top Middle Bottom

Overall average change: -0.0003(-0.008)

Piston Ring End Gap Change

Ring Number	<u>1L</u>	<u>2L</u>	<u>3L</u>	<u>1R</u>	<u>2R</u>	<u>3R</u>	Average Change
1	+0.002(0.05)	+0.005(0.13)	+0.001(0.03)	0.000	+0.004(0.10)	+0.008(0.20)	+0.003(0.08)
2	0.000	0.000	+0.001(0.03)	0.000	-0.002(-0.05)	0.000	0.000
3	+0.002(0.05)	0.000	0.000	0.000	0.000	+0.001(0.03)	+0.001(0.03)
4	+0.001(0.03)	-0.002(-0.05)	+0.001(0.03)	0.000	0.000	+0.001(0.03)	0.000
5	+0.006(0.15)	+0.033(0.84)	+0.006(0.15)	+0.010(0.25)	+0.005(0.13)	+0.098(2.49)	+0.026(0.66)
6	+0.003(0.08)	+0.036(0.91)	+0.004(0.10)	+0.005(0.13)	+0.002(0.05)	+0.013(0.33)	+0.011(0.28)
7	+0.003(0.08)	+0.033(0.84)	+0.002(0.05)	+0.005(0.13)	+0.002(0.05)	+0.015(0.38)	+0.010(0.25)

Overall average change: +0.009(0.23)

^{*}All dimensions are given in inches (mm).

^{##}T-AT = Thrust-Antithrust Direction; F-B = Front-Back Direction. ###Not included in averages.

6V-53T TEST 32

Lubricant: AL-12272-L

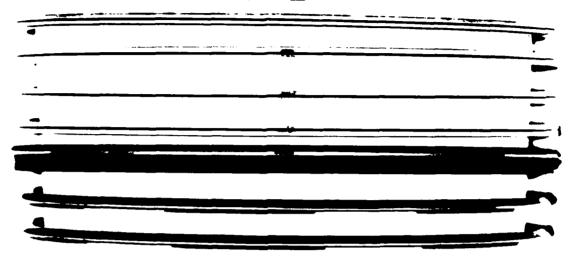
POST TEST ENGINE CONDITION AND DEPOSITS

A. Cylinder Liner							
Intake Port Plugging,	<u> 1L</u>		<u> 3L</u>	<u> 1R</u>		<u>3R</u>	Average
I restriction	<1	<1	<1	<1	<1	<1	<1
Liner Scuffing,							
Z Area					•	100	
Thrust Anti-Thrust	3 1	41 88	4 17	1	3 12	100 100	25.83 36.50
I Total Area Scuffing	ž	64.5	10.5	2.5	7.5	100	31.17
- -						OVERALL:	31.17
% Area Bore Polished							
Thrust	1	0	0	0	1	0	0.33
Anti-Thrust Z Avg. Area Bore	1	0	0	2	2	0	0.83
Polished	1	0	0	1	1.5	0	0.58
						OVERALL:	0.58
B. Pistons							
Ring Face Distress,							
No. 1	24.00	43.25	22.75	15.75	4.00	72.50	30.38
No. 2	1.25	63.75	12.50	0.00	27.75	35.00	23.38
No. 3	2.75	58.75	27.50	0.00	27.50	36. 25	25.46
No. 4	2.00	65.00	21.25	0.00	33.75	33.75 OVERALL:	25.96 24.42
							• • • • • •
Piston Skirt Rating Thrust	S#	70%SC	S	s	s	35 2 SC	
Anti-Thrust	s- s	45%SC	20 7 SC	S	Š	15 2 SC	
Piston WTD Rating**	229.88	168.38	197.50	163.88	223.25	231.88	202.46
Ring Sticking							
No. 1	Pass	CF	F	F	F	CF	
No. 2	F	F	F	ŗ	ŗ	F	
No. 3 No. 4	F F	F F	? ?	P P	P P	? F	
C. Exhaust Valves							
Deposits Head			k +0.1	AHC+			
Face	-			ic		→	
Tulip	•		lyA1	HC ——		-	
Stem	-	~ ~	- #9 Lac	dne 1++		-	
Surface Condition	_	_	_	_	_	_	
Freeness in Guide Head	P .	F	F Normal	<u> </u>	F		
Face	-		Normal-			-	
Seat	•		Normal			-	
Stem Tip			Normal Normal			*	
D. Other Ratings							
Upper Oil Control Ring Expansive Force.							
lbs.	19.2	19.8	20.0	20.0	19.2	20.0	19.7
Bearing Surface Conditi		ir flakin	off and	almost to	noint a	f melting;	remainin
	bearing	had scri	tches wi	th #4 shor	ving copp	er.	
Rod Bearings				ing beari	ngs have	scratches	and some
Cam Bearings		imbedded : few scrate					
*L * Light, \$ = Scratch	nes. PM -	Platine !	telted. N	- Normal	SC - Sc	uffipe. B	- Burn
**CRC Weighted Total De	posits (0 = least,	, 900 = w	ost)			
***HS = Hotstuck, CS Cold Stuck, P = Pinched, F = Free, N = Normal, C = Chipped +HC = Hard Carbon; the number-letter, prefix indicates carbon depth with							

⁺HC = Hard Carbon; the number-letter, prefix indicates carbon depth with $\frac{1}{12}A$ = least to J = most ++= The higher the number, the darker the lacquer (0 = lightest, 9 = darkest)

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6V53T(#32) 1-L



6V53T(#32) 1-R



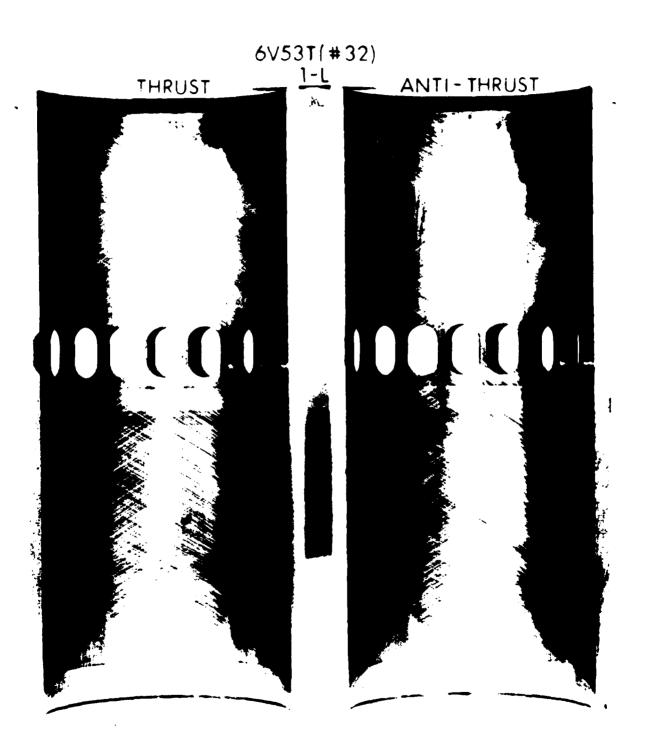




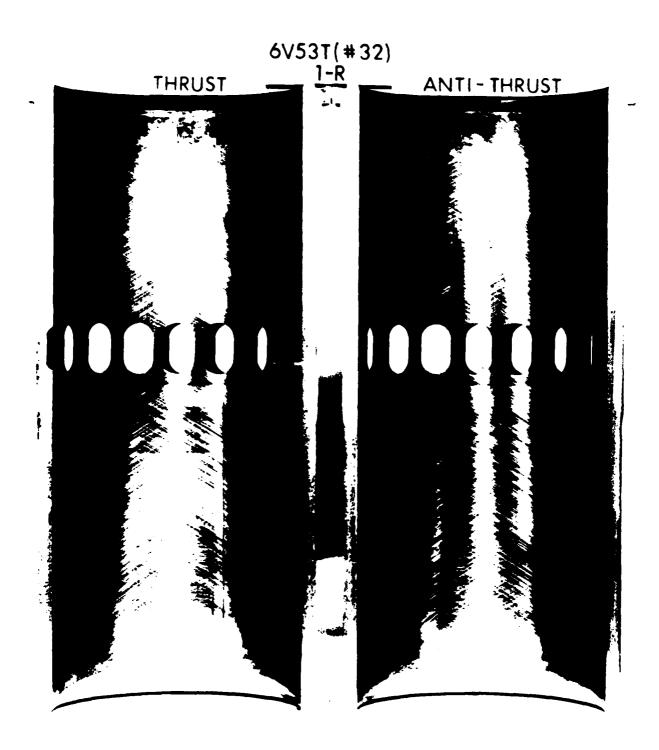
6V53T(#32) 1-R-AT

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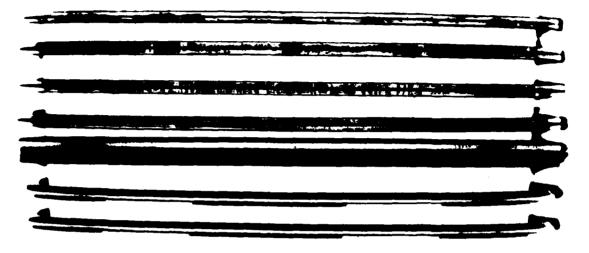




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6V53T(#32) 2-L



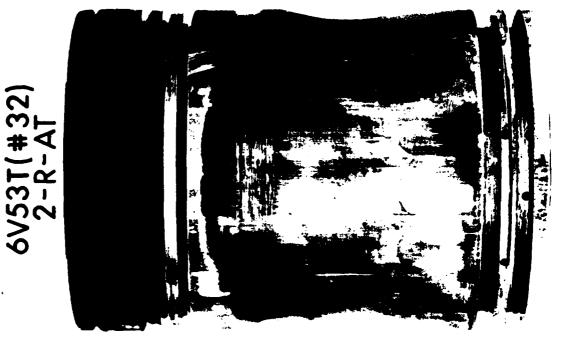
6V53T(#32) 2-R





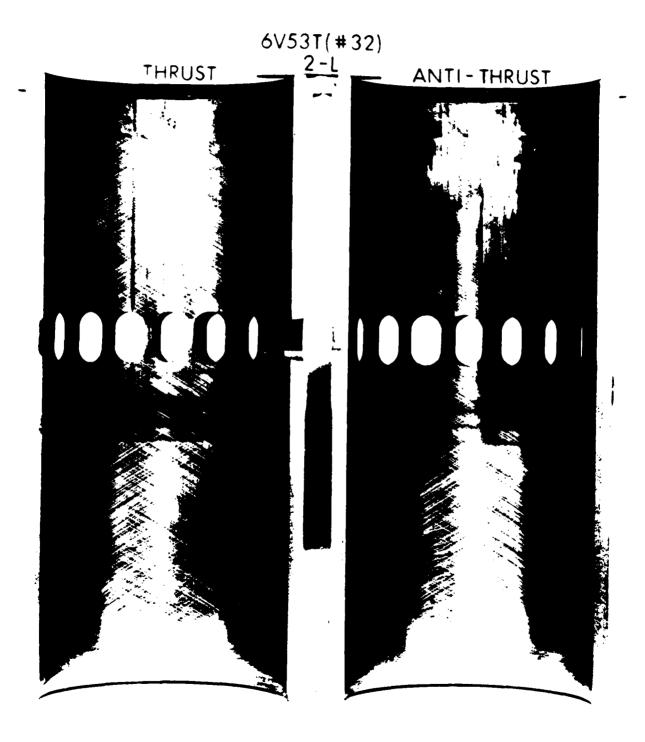


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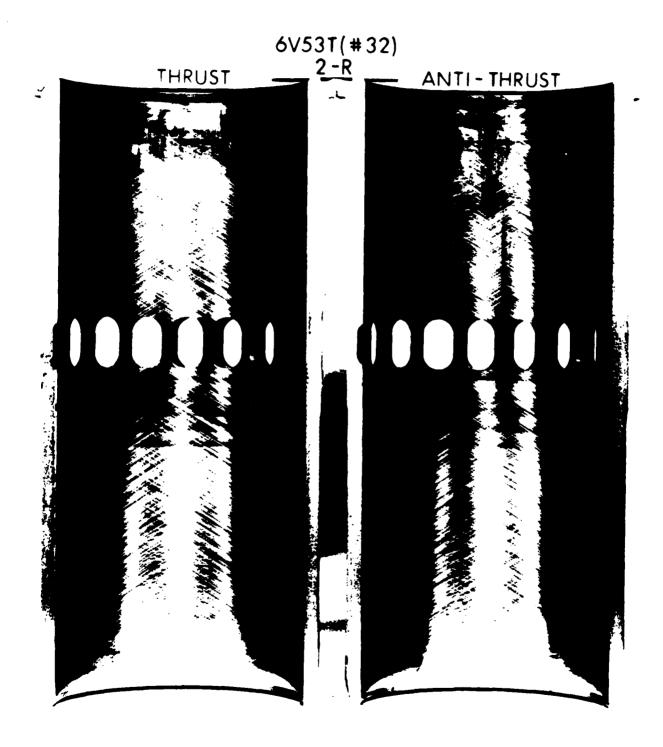


6V53T(#32) 2-R-T

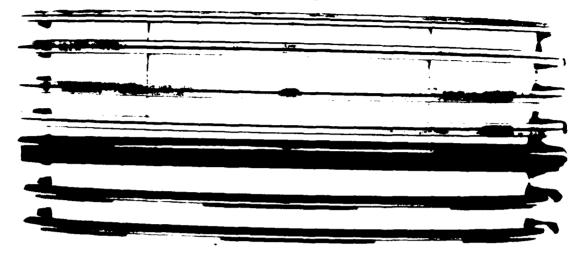
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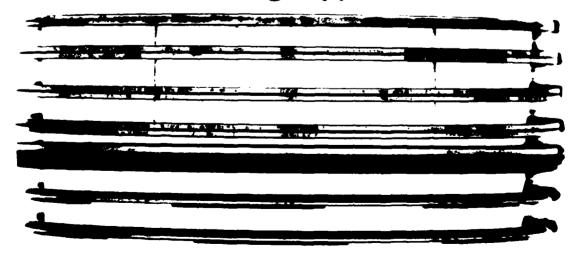
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6V53T(#32) 3-L



6V53T(#32) 3-R





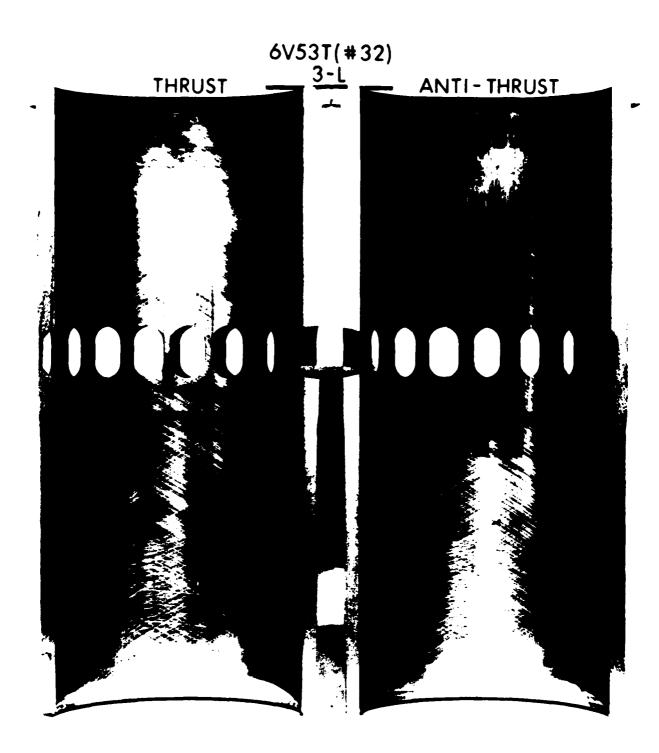
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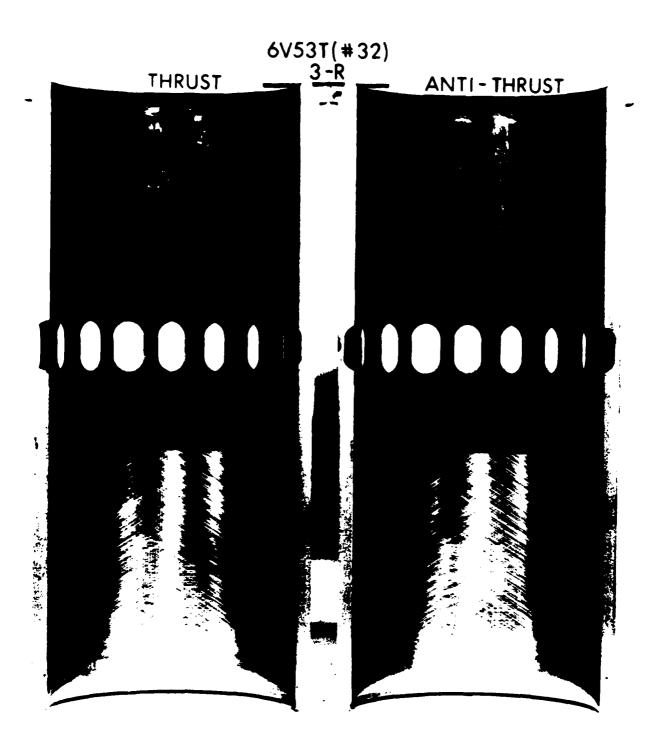
6V53T(#32) 3-R-AT

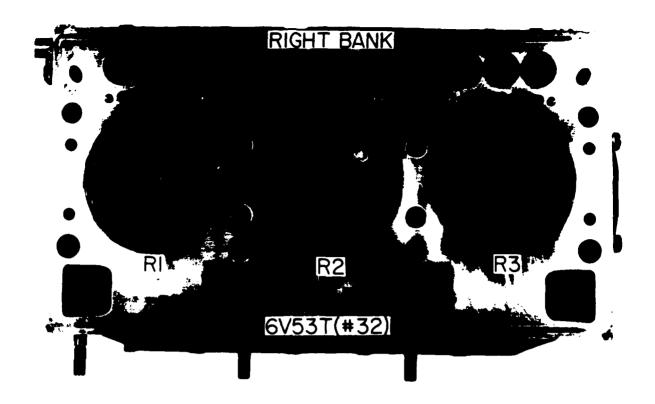
6V53T(#32) 3-R-T

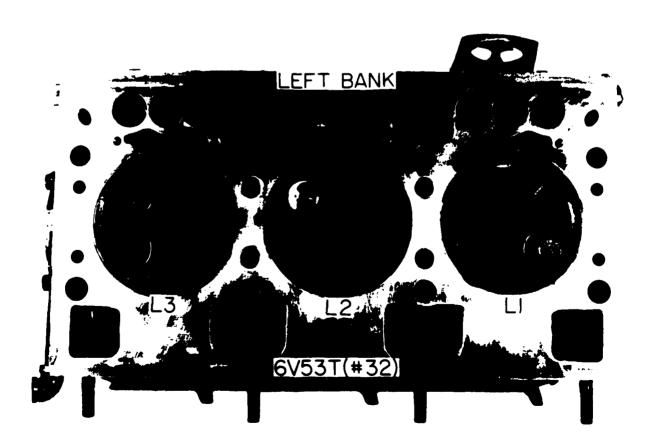




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APPENDIX D

ENGINE-LUBRICANT COMPATIBILITY TEST 240-HOUR TRACKED-VEHICLE CYCLE USING 6V-53T DIESEL FUEL

Lubricant AL-12271-L, Test No. 34

ENGINE-LUBRICANT COMPATIBILITY TEST 240-HOUR TRACKED-VEHICLE CYCLE USING 6V-53T DIESEL ENGINE

Test Lubricant: AL-12272-L Test Fuel: Caterpillar 1-H Engine Test Number: 34 Date Completed: 30 August 1983

Conducted For

U.S. Army Mobility Equipment Research and Development Command Materials, Fuels and Lubricants Fort Belvoir, Virginia

Ву

U.S. Army Fuels and Lubricants Research Laboratory
Southwest Research Institute
San Antonio, Texas 78284

6V-53T TEST 34 ENCINE REBUILD MEASUREMENTS* Model Number: 5063-5395 Serial Number: 6D-157211

	Min	Hax	Ava	Spec	Specified Limits
Cylinder Block Bore					
Inside Diameter (Bottom)	4.3565(110.655)	4.3580(110.693)	4.3573(110.675)	4.3565(110.655)	
Out-of-Round Taper	0.000	0.0011(0.028) 0.0010(0.025)	0.0004(0.010) 0.0004(0.010)		- 4.5595(110./51) Max - 0.0015(0.038) Max - 0.0015(0.038) Max
Cylinder Liners (Installed) Inside Diameter Out-of-Round Taper	3.8756(98.440) 0.0000 0.0000	3.8766(98.466) 0.0004(0.010) 0.0006(0.015)	3.8761 (98.454) 0.0001 (0.003) 0.0001 (0.003)	3.8752(98.430)	- 3.8767(98.468) - 0.0015(0.038) Max - 0.0015(0.038) Max
Piston Diameter (at skirt)	3.8679 (98.245)	3.8688(98.268)	3.8682 (98.252)	3.8669(98.219)	- 3.8691(98.775)
Piston Skirt to Cylinder Liner Clearance	0.0073(0.185)	0.0084 (0.213)	0,0080(0,203)	0.0061 (0.155)	- 0.0098(0.249)
Compression Rings Gap (No. 1, Fire Ring) Gap (Nos. 2, 3, 4)	0.029(0.74) 0.029(0.74)	0.036(0.91) 0.036(0.91)	0.033(0.84) 0.032(0.81)	0.020(0.51) 0.020(0.51)	- 0.046(1.17) - 0.036(0.91)
Ring-to-Groove Clearance** Top (No. 1, Fire Ring) No. 2, Compression Ring	_ 0.003(0.08) 0.007(0.18)	0.004(0.10) 0.008(0.20)	0.004(0.10) 0.008(0.20)	0.003(0.08) 0.007(0.18)	- 0.006(0.15) - 0.010(0.25)
No. 3 and 4, Compression Rings	0.005(0.13)	0,007(0,18)	0.006(0.15)	0.005(0.13)	- 0.008(0.20)
Oil Control Rings, Mos. 5, 6, 7 Cap Ring-to-Groove Clearance	0.016(0.41)	0.022(0.56) 0.004(0.10)	0.018(0.46)	0.010(0.25) 0.0015(0.038)	- 0.025(0.64) - 0.0055(0.140)
Piston Pin Pin-to-Piston Bushing Clearance	0,0030(0,076)	0.0033(0.084)	0.0032(0.81)	0.0025(0.064)	- 0.0034(0.086)
Fin-fo-Connecting Kod Bushing Clearance	0.0014(0.036)	0.0018(0.046)	0.0016(0.041)	0.0010(0.025)	- 0.0019(0.048)
Connecting Rod Bearing- to-Journal Clearance	0.0022(0.056)	0.0029(0.074)	0.0025(0.064)	0,0011(0,028)	- 0.0041(0.104)
Main Bearing-to-Journal Clearance	0,0032(0,081)	0.0033(0.084)	0,00 13(0,084)	0.0010(0.025)	- 0.0040(0.102)
Camshaft Bearing-to- Journal Clearance	0,0050(0,127)	0.0054(0.137)	0*003(0*130)	0.0045(0.114)	- 0.0060(0.152)

6V-5ST 240-HOUR TRACKED VEHICLE CYCLE BEFORE AND AFTER TEST 34 PERFORMANCE DATA **POWER** Before test 0 ---- 0 After test ₹ ENGINE SPEED-RPM BMEP Before test 0 --- 0 g 1000 5 ENGINE SPEED-RPM **BSFC** Before test 0 ---- 0 0.42 0.38

ENGINE SPEED-RPM

6V-53T 240-HOUR TRACKED VEHICLE CYCLE ENDURANCE TEST TEST 34 OPERATING CONDITIONS SUMMARY

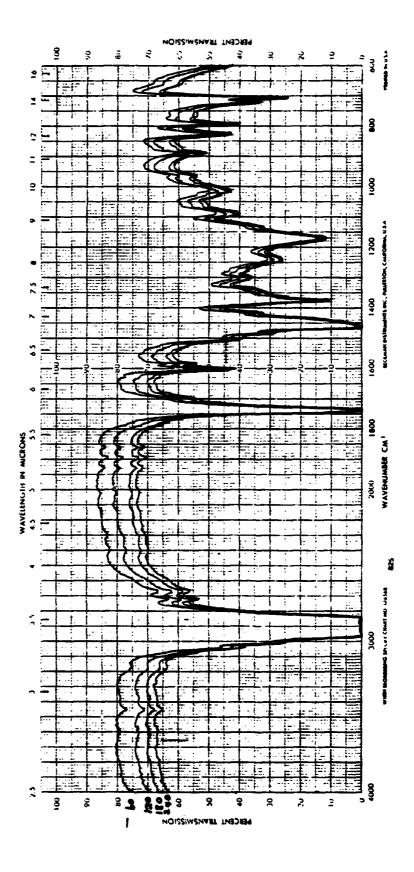
Lubricant: AL-12272-L Fuel: Caterpillar 1-H

	Maximum Po		Maximum Torque Mode (2200 RPM)		
	Mean	Standard Deviation	Mean	Standard Deviation	
Engine Speed, rpm	2800	5.52	2200	4.77	
Torque, ft-1b (N-m)	439 (596)	2.99(4.05)	492(667)	10.90(14.8)	
Fuel Consumption, 1b/hr(kg/hr)	93.4(42.4	0.993(0.45)	77.1(35)	1.53(0.69)	
Observed Power, Bhp(kW)	234(175)	1.62(1.21)	206 (154)	4.60(3.44)	
BSFC, 1b/Bhp-hr(g/kW-hr)	0.400(243)	0.004(2.61)	0.375(228)	0.007(4.31)	
Temperatures, °F(°C)					
Exhaust before Turbo	864 (462)	22.60(12.6)	824(440)	23.40(13)	
Exhaust after Turbo	711 (377)	18.60(10.3)	729 (387)	22.80(12.7)	
Water Jacket Inlet	158(70.2)	1.97(1.10)	158(69.7)	1.16(0.64)	
Water Jacket Outlet	170(76.8)	1.88(1.05)	170 (76.4)	1.22(0.68)	
Oil Sump	227(109)	2.23(1.24)	220(104)	2.31(1.28)	
Fuel at Filter	94(34.6)	2.60(7.95)	91.4(33)	4.18(2.32)	
Inlet Air	98(36.5)	4.58(2.55)	96.8(36)	4.21(2.34)	
Airbox	258 (125)	5.34(2.96)	216(102)	3.95(2.20)	
Pressures					
Exhaust before Turbo,					
psi(kPa)	10.48(72.3)	0.09(0.62)	6.92(47.7)	0.12(0.84)	
Exhaust after Turbo,					
in. Hg(kPa)	2.03(6.85)	0.89(3.01)	1.29(4.34)	0.45(1.50)	
Compressor Discharge, psi(kPa)	10.33(71.2)	0.23(1.56)	7.00(48.3)	0.20(1.35)	
Blower Discharge, psi(kPa)	15.06(104)	0.44(3.05)	8.39(57.9)	0.49(3.40)	
Oil Gallery, psi (kPa)	51.75(357)	0.41(2.83)	45.1(311)	0.58(3.99)	
Intake Vacuum, in. H ₂ O(kPa)	6.78(1.69)	0.16(0.04)	3.89(0.97)	0.12(0.03)	
Ambient Conditions					
Dry Bulb Temperature, °F(°C)	83.1(28.4)	5.38(2.99)	83.2(28.4)	4.87(2.71)	
Wet Bulb Temperature, °F(°C) Barometric Pressure,	77.6(25.3)	7.09(3.94)	77.3(25.2)	6.42(3.56)	
<pre>in. Hg(kPa) (Both modes of operation)</pre>	29.1(98.3)	0.09(0.30)			

^{*68%} of the values for a given variable occur within ±1 standard deviation of the mean; 95% occur within ±2 standard 'eviations.

	- -	240	29.87	5.82	2.32	4.30	0.07	90°0	229
		220	1	5.82	1	1	1	1	1
		700	1	5.83	1	1	1	1	1
		28	29.78	5.82	2.31	4.22	90.0	0.05	f
		160	1	5.73	. 1	1	1	1	1
	Hours	140	;	5.84	i	ł	ł	;	ł
33.5	Time.	120	30.42	5,91	2,25	3.00	90°0	0.05	232
T 34 ANALYSIS AL-12-27-1		100	1	5.88	ı	;	ł	1	1
E - 1		80	1	5.89	;	!	1	¦	}
6V-5 TEST LUBRICANT		09	30,32	5.77	2.20	3,30	0.02	0.02	1
	3	07	1	5.89	1	1	1	1	` }
		2	· 	5.95	1	· 	· 	, 	
		0	32.0	6.37	2.10	- 16°2	• 0•0	0.0	- 622
	ASTM Test	Method	D 445 3	D 445 6	D 664 2	D 664 7	D 893 0	D 893 0	
	∀ Ĥ	윘		y cSt D	۵	Q			D 92
			viscosity (104°F) cSt	viscosity (212°F) c	Number	Number	Pentane B Insolubles	Toluene B Insolubles	္ ့
			Kinem:tic viscosity at 40°C (104°F) c	Kinematic viscosity at 100°C (212°F)	Total Acid Number mg KOH/g	C Total Base Number G mg KOH/g	entane B I	oluene B I	Flash Point,
			Ž.	Z	Ţ	₽ D-5	R	Τ	FI
		Š.					<u> </u>		

INFRARED SPECTRUM
6V-53T
TEST 34
LUBRICANT: AL-12272-L



A second Associated (seconds A seconds A seconds A barbara A second A second

6V-53T TEST 34 Lubricant: AL-12272-L

TOTAL CONSUMPTION AND WEAR METALS BY XRF

			Wear Me	tals, ppm
Test Time, Hours	Total Oil Con	sumed, 1b(kg)	Fe	Cu
0			44	<10
20	6.80	(3.08)	77	<10
40	14.50	(6.58)	83	<10
60	23.30	(10.57)	89	17
87	30.12	(13.66)	70	<10
100	39.88	(18.09)	83	<10
120	Oil Change		81	15
140	46.32	(21.01)	37	<10
160	57.41	(26.04)	47	<10
173	60.78	(27.57)		
180	72.06	(32.69)	68	<10
185.5	79.19	(35.92)		
187.5	86.55	(39.26)		
190	93.81	(42.55)		
200	106.75	(48.42)	157	<10
220	116.54	(52.86)	128	< 10
240	129.63	(58.80)	110	<10
185.5 187.5 190 200 220	79.19 86.55 93.81 106.75 116.54	(35.92) (39.26) (42.55) (48.42) (52.86)	157 128	<10 <10

Average oil consumption rate: 0.54 lb/hr (0.24 kg/hr)

6V-53T TEST 34

Lubricant: AL-12272-L

WEAR MEASUREMENTS*

Cylinder Liner Bore Diameter Change

		<u>1L</u>	Cylinder	Number 2L		<u>3L</u>
	<u>T-AT**</u>	<u>F-B</u>	<u>T-AT</u>	<u>F-B</u>	<u>T-AT</u>	<u>F-B</u>
Top Middle Bottom	+0.0007 (0.018) +0.0004 (0.010) 0.0000	+0.0002 (0.005) -0.0003 (-0.008) -0.0005 (-0.013)	+0.0004 (0.010) 0.0000 +0.0007 (0.018)	+0.0001 (0.003) -0.0001 (-0.003) +0.0001 (0.003)	+0.0014 (0.036) +0.0004 (0.010) +0.0002 (0.005)	-0.0003 (-0.008) -0.0002 (-0.005) +0.0001 (0.003)
	<u>1R</u>		Cylinder 21		<u>3R</u>	
	T-AT*	<u>F-B</u>	<u>T-AT</u>	<u>F-B</u>	T-AT	<u>F-B</u>
Top Middle Bottom	+0.0018(0.046) +0.0004(0.010) -0.0003(-0.008)	+0.0002(0.005) +0.0003(0.008) +0.0001(0.003)	-0.0001(-0.003) +0.0005(0.013) -0.0001(-0.003)	+0.0006(0.015) +0.0004(0.010) -0.0003(-0.008)	+0.0039(0.099) +0.0017(0.043) +0.0001(0.003)	+0.0031(0.079) +0.0014(0.036) 0.0000

Average Change

	<u>T-AT</u>	<u>F-B</u>
Top Middle	+0.0014 (0.036) +0.0006 (0.015)	+0.0007 (0.018) +0.0003 (0.008)
Bottom	+0.0001 (0.003)	-0.0001 (-0.003)

Overall average change: +0.0005 (0.013)

Piston Ring End Gap Change

Ring Number	<u>1L</u>	<u>2L</u>	<u>3L</u>	<u>1R</u>	<u>2R</u>	<u>3R</u>	Average Change
1	0.000	0.000	+0.001(0.03)	+0.001(0.03)	0.000	+0.007(0.18)	+0.002(0.05)
2	0.000	-0.001(-0.03)	+0.001(0.03)	0.000	0.000	0.000	0.000
3	0.000	0.000	+0.001(0.03)	0.000	0.000	-0.003(-0.08)	0.000
4	0.000	0.000	+0.001(0.03)	0.000	0.000	-0.001(-0.03)	0.000
5	+0.006(0.15)	+0.004(0.10)	+0.004(0.10)	+0.006(0.15)	+0.006(0.15)	+0.012(0.30)	+0.006(0.15)
6	0.000	+0.001(0.03)	0.000	+0.002(0.05)	+0.004(0.10)	+0.006(0.15)	+0.002(0.05)
7	0.000	0.000	-0.001(-0.03)	+0.005(0.13)	+0.002(0.05)	+0.003(0.08)	+0.002(0.05)

Overall average change: +0.002(0.05)

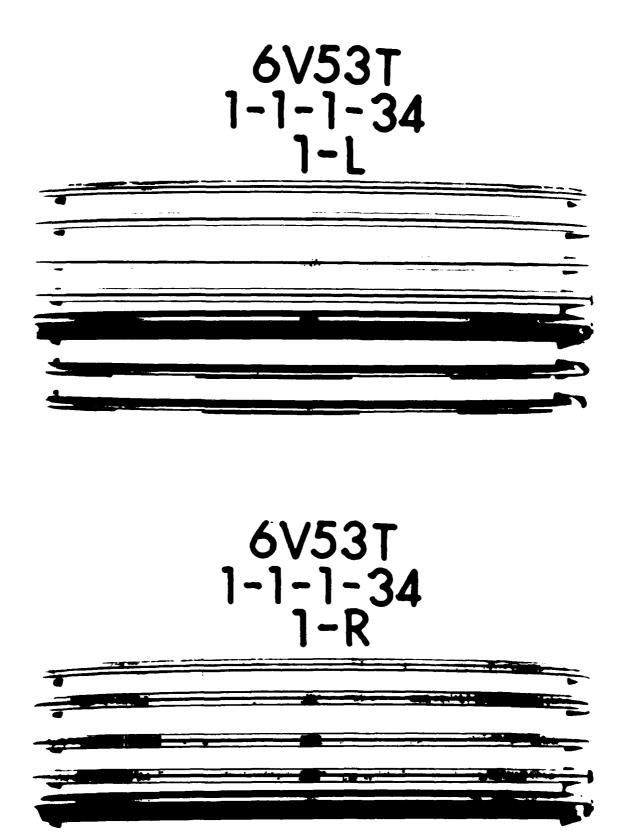
^{*}All dimensions are given in inches (mm).

**T-AT = Thrust-Antithrust Direction; F-B = Front-Back Direction.

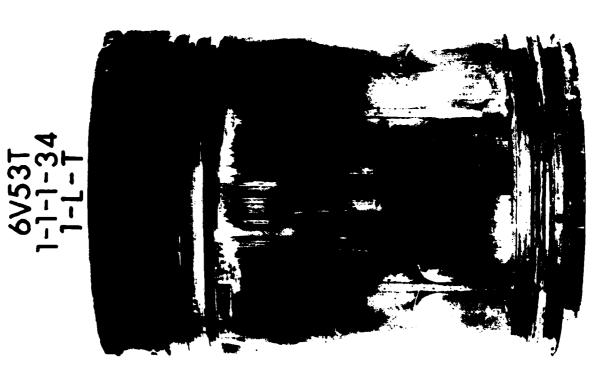
6V-53T TEST 34 Lubricant: AL-12272-L POST TEST ENGINE CONDITION AND DEPOSITS

	lL	2L	3L	1R	2R	3R	Average
A. Cylinder Liner							
Intake Port Plugging. Z restriction	<1	<1	<1	<1	<1	<1	<1
Liner Scuffing,							
2 Area							
Thrust	3.00	0.00	26.00	88.00	43.00	100.00	43.33
Anti-Thrust	2.00	5.00	9.00	26.00	23.00	82.00	24.50
Z Total Area Scuffed	2.50	2.50	17.50	57.00	33.00	91.00	33.92
						Overall:	33.92
% Area Bore Polished							
Thrust	1.00	1.00	1.00	0.00	2.00	0.00	0.83
Anti-Thrust	5.00	2.00	2.00	7.00	2.00	1.00	3.17
Z Avg. Area Bore							
Polished	3.00	1.50	1.50	3.50	2.00	0.50 Overall:	2.00 2.00
B. Pistons							
Ring Face Distress,							
(demerits)	10.50	0.66	20.25	25 25	20.50	65.00	20 22
No. 1	10.50	9.50	29.25	25.25	30.50	65.00	28.33
No. 2	0.00	1.50	14.25	34.00	17.75	55.00	20.42
No. 3	0.00	1.00	28.75	32.50	25.00	61.25	24.75
						Overall:	24.50
D4 - Chi 04							
Piston Skirt Rating	c •		15%SC	10800	E#CC	25850	
Thrust	S*	S		40%SC	5%SC	35%SC	
Anti-Thrust	S	S	S	5%SC	< 5%SC	30 % SC	
Piston WTD Rating**	242.50	220.75	240.63	225.88	200.00	266.38	232.69
Ring Sticking							
Ring Sticking No. 1			Fre	e ——			
	-					→	
No. I	-			e		→	
No. 1 No. 2 No. 3	-	<u>-</u>	Fre	e	·	→	
No. 1 No. 2			Fre	e		→	
No. 1 No. 2 No. 3 C. Exhaust Valves	-		Fre	e		→	
No. 1 No. 2 No. 3 C. Exhaust Valves			Fre	e		→	
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head	BHC+	AHC	Fre Fre	CHC	внс	AHC	
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head Face	½AHC	LAHC	Fre Fre SAHC SAHC	CHC LAHC	AHC	AHC	
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head Face Tulip	LAHC LAHC	SAHC	SAHC SAHC SAHC SAHC	CHC LAHC LAHC	LAHC LAHC	LAHC LAHC	
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head Face	LAHC LAHC LAHC	LAHC LAHC LAHC	SAHC SAHC SAHC SAHC SAHC SAHC	CHC ZAHC ZAHC ZAHC	LAHC LAHC LAHC	Lahc Lahc Lahc	
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head Face Tulip	LAHC LAHC	SAHC	SAHC SAHC SAHC SAHC	CHC LAHC LAHC	LAHC LAHC	LAHC LAHC	
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head Face Tulip Stem	LAHC LAHC LAHC	LAHC LAHC LAHC	SAHC SAHC SAHC SAHC SAHC SAHC	CHC ZAHC ZAHC ZAHC	LAHC LAHC LAHC	Lahc Lahc Lahc	
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head Face Tulip Stem Surface Condition	LAHC LAHC LAHC #9++	LAHC SAHC LAHC #9	SAHC SAHC SAHC SAHC SAHC SAHC SAHC SAHC	CHC VAHC VAHC VAHC VAHC VAHC	LAHC LAHC LAHC 19	tahc tahc tahc #9	
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head Face Tulip Stem Surface Condition Freeness in Guide	LAHC LAHC LAHC	LAHC LAHC LAHC	SAHC SAHC SAHC SAHC SAHC SAHC SAHC	CHC ZAHC ZAHC ZAHC	LAHC LAHC LAHC	Lahc Lahc Lahc	
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head Face Tulip Stem Surface Condition Freeness in Guide Head	LAHC LAHC LAHC #9++	LAHC SAHC LAHC #9	SAHC VAHC VAHC VAHC VAHC VAHC VAHC VAHC V	CHC VAHC VAHC VAHC VAHC VAHC	LAHC LAHC LAHC 19	tahc tahc tahc #9	
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head Face Tulip Stem Surface Condition Freeness in Guide Head Face	LAHC LAHC LAHC #9++	LAHC SAHC LAHC #9	YAHC YAHC YAHC YAHC YAHC YAHC YAHC YOUR YOUR YOUR YOUR NOTES 1	CHC HAHC HAHC HAHC HAHC #9	LAHC LAHC LAHC 19	tahc tahc tahc #9	
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head Face Tulip Stem Surface Condition Freeness in Guide Head Face Seat	LAHC SAHC LAHC #9++	SAHC SAHC SAHC 99	SAHC VAHC VAHC VAHC VAHC VAHC VAHC VAHC V	CHC YAHC YAHC YAHC YAHC #9	FAHC	EAHC EAHC EAHC #9	
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head Face Tulip Stem Surface Condition Freeness in Guide Head Face Seat Stem	LAHC SAHC LAHC #9++	LAHC SAHC LAHC #9	AHC LAHC LAHC M9 F Normal L Normal L Normal o heavy w	CHC LAHC LAHC #9	FAHC	EAHC EAHC EAHC #9	
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head Face Tulip Stem Surface Condition Freeness in Guide Head Face Seat	LAHC SAHC LAHC #9++	SAHC SAHC SAHC 99	SAHC VAHC VAHC VAHC VAHC VAHC VAHC VAHC V	CHC LAHC LAHC #9	FAHC	EAHC EAHC EAHC #9	
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head Face Tulip Stem Surface Condition Freeness in Guide Head Face Seat Stem	LAHC SAHC LAHC #9++	SAHC SAHC SAHC 99	AHC LAHC LAHC M9 F Normal L Normal L Normal o heavy w	CHC LAHC LAHC #9	FAHC	EAHC EAHC EAHC #9	
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head Face Tulip Stem Surface Condition Freeness in Guide Head Face Seat Stem Tip D. Other Ratings	LAHC SAHC LAHC #9++	SAHC SAHC SAHC 99	AHC LAHC LAHC M9 F Normal L Normal L Normal o heavy w	CHC LAHC LAHC #9	FAHC	EAHC EAHC EAHC #9	
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head Face Tulip Stem Surface Condition Freeness in Guide Head Face Seat Stem Tip	LAHC SAHC LAHC #9++	SAHC SAHC SAHC 99	AHC LAHC LAHC M9 F Normal L Normal L Normal o heavy w	CHC LAHC LAHC #9	FAHC	EAHC EAHC EAHC #9	19.6
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head Face Tulip Stem Surface Condition Freeness in Guide Head Face Seat Stem Tip D. Other Ratings Upper Oil Control Ring Expansive Force, lbs.	EAHC SANC FLANC #9++	EAHC SAHC SAHC #9	SAHC SAHC SAHC SAHC SAHC SAHC SAHC SAHC	CHC HAHC HAHC HAHC HAHC #9	F scuffing	EAHC EAHC EAHC 99	19.6
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head Face Tulip Stem Surface Condition Freeness in Guide Head Face Seat Stem Tip D. Other Ratings Upper Oil Control Ring Expansive Force, 1bs. Bearing Surface Conditi	F Some	F medium t	Free Lanc Lanc Market Lanc Lanc Market Lanc Lanc Market Lanc Market Lanc Lanc Lanc Lanc Lanc Lanc Lanc Lanc	CHC LAHC LAHC LAHC #9	F scuffing	F 19.4	19.6
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head Face Tulip Stem Surface Condition Freeness in Guide Head Face Seat Stem Tip D. Other Ratings Upper Oil Control Ring Expansive Force, 1bs. Bearing Surface Condition Main Bearings	F Some	EAHC SAHC SAHC #9 F medium t	Free AAHC AAHC AAHC AAHC AAHC AAHC AAHC AA	CHC HAHC HAHC HAHC #9 F Tear with	F scuffing 19.4	F 19.4 scratches	
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head Face Tulip Stem Surface Condition Freeness in Guide Head Face Seat Stem Tip D. Other Ratings Upper Oil Control Ring Expansive Force, lbs. Bearing Surface Conditi Main Bearings Rod Bearings	F Some	F medium t 20.0	Free SAHC SAHC SAHC SAHC SAHC SAHC SAHC SAHC	CHC LAHC LAHC LAHC #9 F Tear with	F scuffing 19.4	EAHC LAHC LAHC LAHC H9 F 19.4 scratches est have s	ome scratches
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head Face Tulip Stem Surface Condition Freeness in Guide Head Face Seat Stem Tip D. Other Ratings Upper Oil Control Ring Expansive Force, 1bs. Bearing Surface Condition Main Bearings	F Some 19.2 on 12 main 12 conne 2 camah	F medium t 20.0 bearing octing rod aft bear	Free AHC LAHC LAHC LAHC M9 F Normal Normal Normal Normal Lahc Normal No	CHC LAHC LAHC LAHC LAHC #9 F Tear with	F scuffing 19.4 est have copper; r , wiped	F 19.4 scratches est have s bearing ma	
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head Face Tulip Stem Surface Condition Freeness in Guide Head Face Seat Stem Tip D. Other Ratings Upper Oil Control Ring Expansive Force, lbs. Bearing Surface Conditi Main Bearings Rod Bearings	F Some 19.2 on 12 main 12 conne 2 camah	F medium t 20.0	Free AHC LAHC LAHC LAHC M9 F Normal Normal Normal Normal Lahc Normal No	CHC LAHC LAHC LAHC LAHC #9 F Tear with	F scuffing 19.4 est have copper; r , wiped	F 19.4 scratches est have s bearing ma	ome scratches
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head Face Tulip Stem Surface Condition Freeness in Guide Head Face Seat Stem Tip D. Other Ratings Upper Oil Control Ring Expansive Force, lbs. Bearing Surface Conditi Main Bearings Rod Bearings	F Some 19.2 on 12 main 12 came deposite	F medium t 20.0 bearing octing rod aft bear	Free AHC LAHC LAHC LAHC M9 F Normal Normal Normal Normal Lahc Normal No	CHC LAHC LAHC LAHC LAHC #9 F Tear with	F scuffing 19.4 est have copper; r , wiped	F 19.4 scratches est have s bearing ma	ome scratches
No. 1 No. 2 No. 3 C. Exhaust Valves Deposits Head Face Tulip Stem Surface Condition Freeness in Guide Head Face Seat Stem Tip D. Other Ratings Upper Oil Control Ring Expansive Force, 1bs. Bearing Surface Conditi Main Bearings Rod Bearings Camehaft Bearings	F Some 19.2 on 11. conne #2 camen deposite	F medium t 20.0 bearing cting rodusft bearing it in t	Free SAHC SAHC SAHC SAHC SAHC SAHC SAHC SAHC	CHC LAHC LAHC LAHC #9 F Tear with 19.4 copper; reworn to con housing le of the	F scuffing 19.4 est have copper; rg. wiped; shaft.	F 19.4 scratches est have s bearing ma (Plugged)	ome scratches

^{*}L = Light, S = Scratches, PM = Plating Melted, N = Normal, SC = Scuffing, B = Burn *ACRC Weighted Total Deposits (0 = least, 900 = most)
+HC = Hard Carbon; the number-letter, prefix indicates carbon depth with the = least to J = most ++ = Lacquer; the higher the number, the darker the lacquer (0 = lightest, 9 = darkest)



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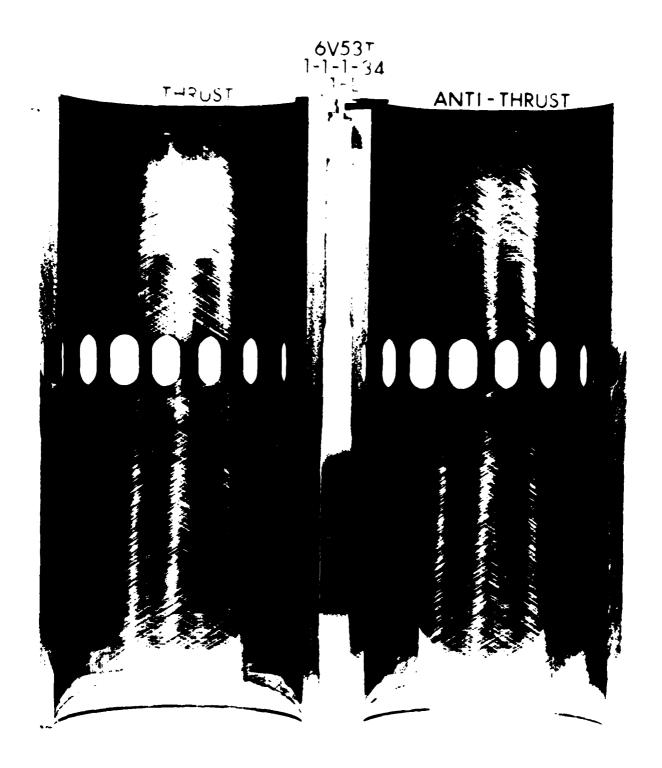


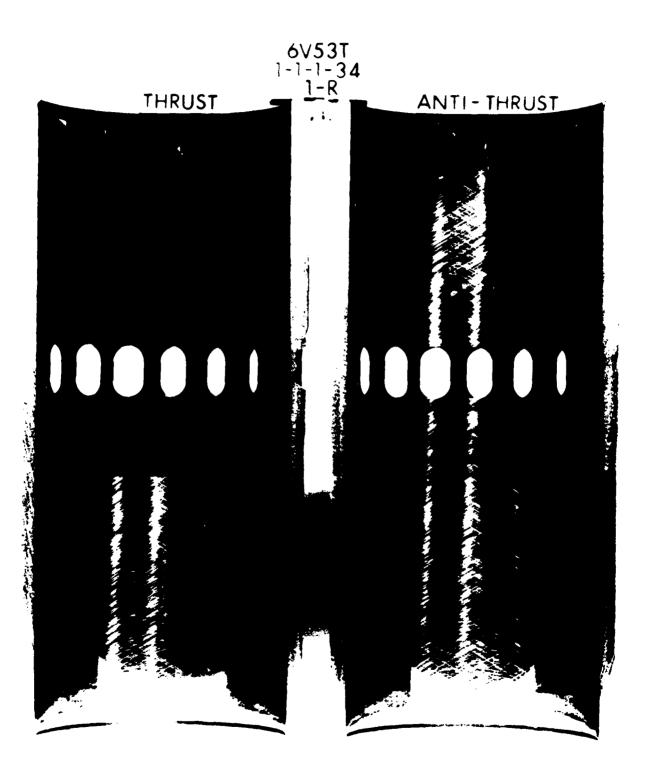
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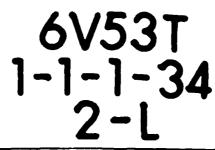
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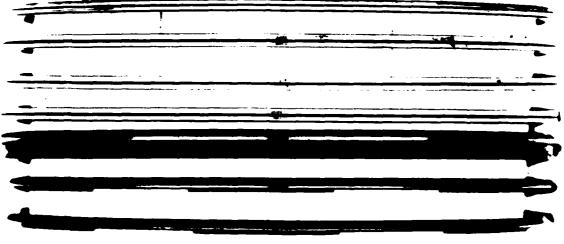
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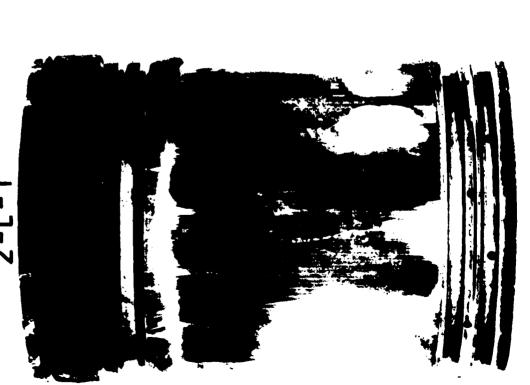


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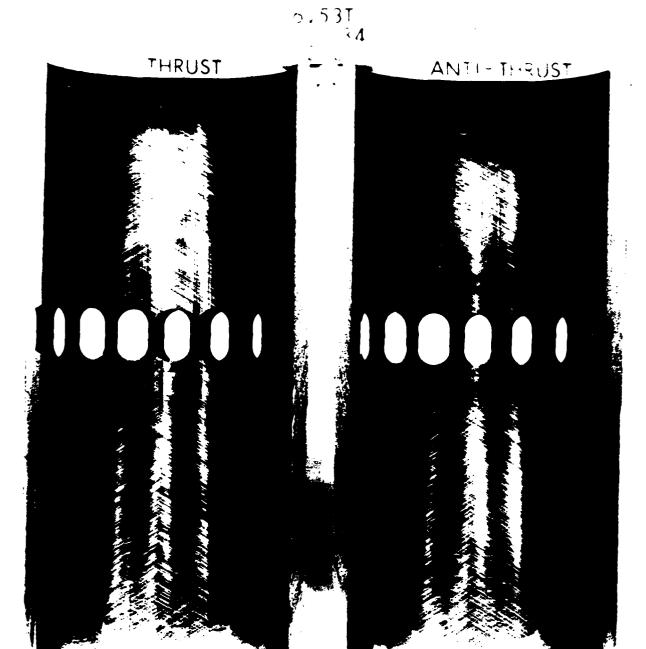


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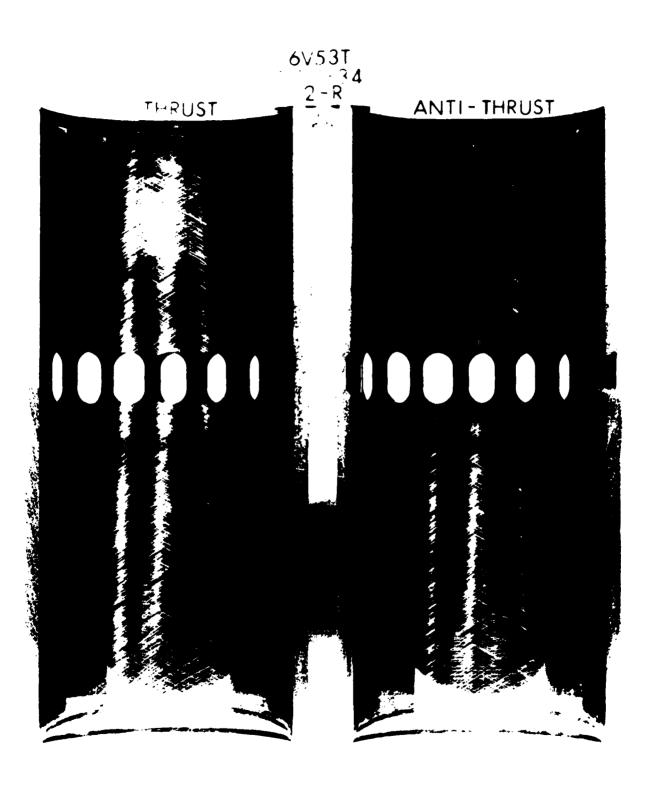
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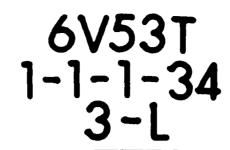


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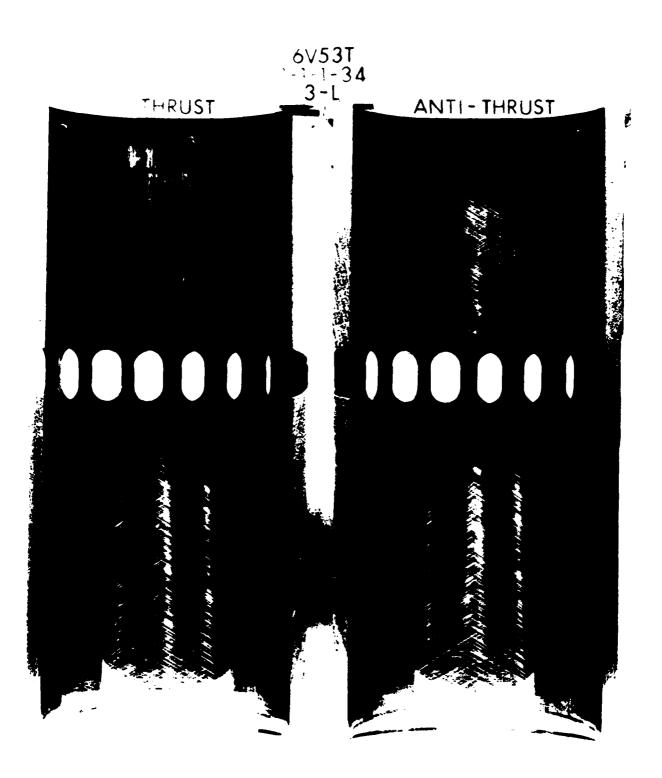


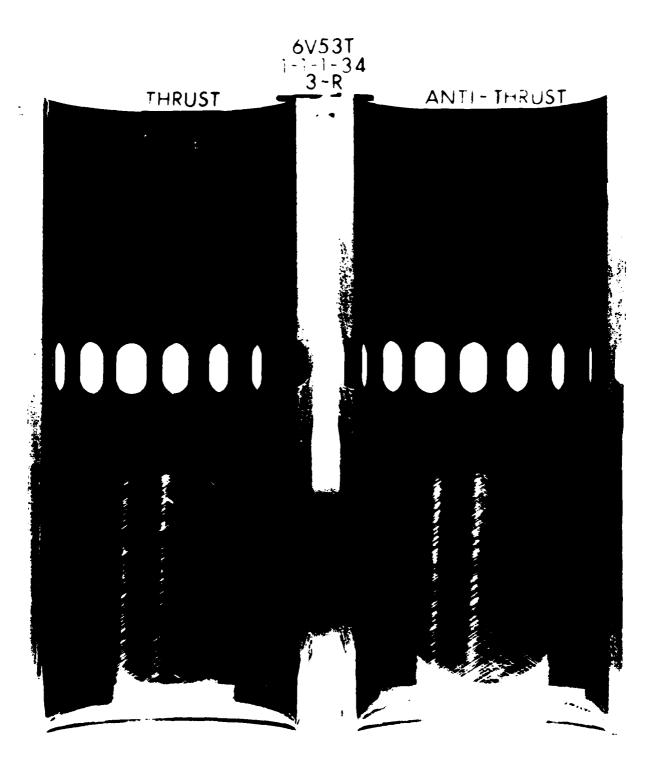
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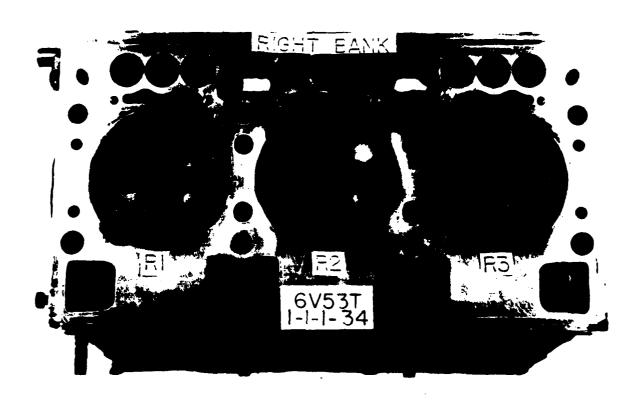
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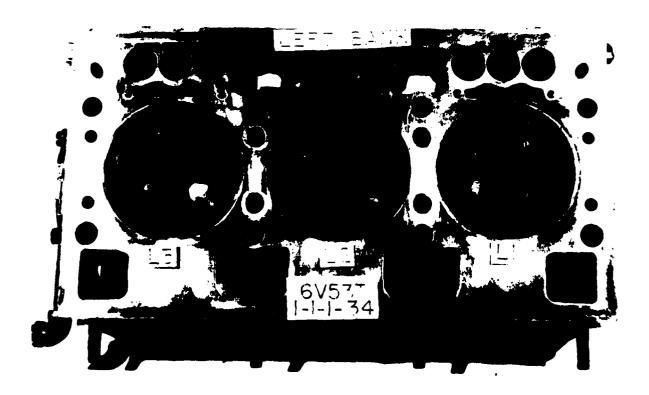


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APPENDIX E

ENGINE-LUBRICANT COMPATIBILITY TEST 240-HOUR TRACKED-VEHICLE CYCLE USING 6V-53T DIESEL FUEL

Lubricant AL-12186-L, Test No. 35

ENGINE-LUBRICANT COMPATIBILITY TEST 240-HOUR TRACKED-VEHICLE CYCLE USING 6V-53T DIESEL ENGINE

Test Lubricant: AL-12186-L
Test Fuel: Caterpillar 1-H
Engine Test Number: 35*
Date Completed: 12 September 1983

Conducted For

U.S. Army Mobility Equipment Research and Development Command
Materials, Fuels and Lubricants
Fort Belvoir, Virginia

Ву

U.S. Army Fuels and Lubricants Research Laboratory Southwest Research Institute San Antonio, Texas 78284

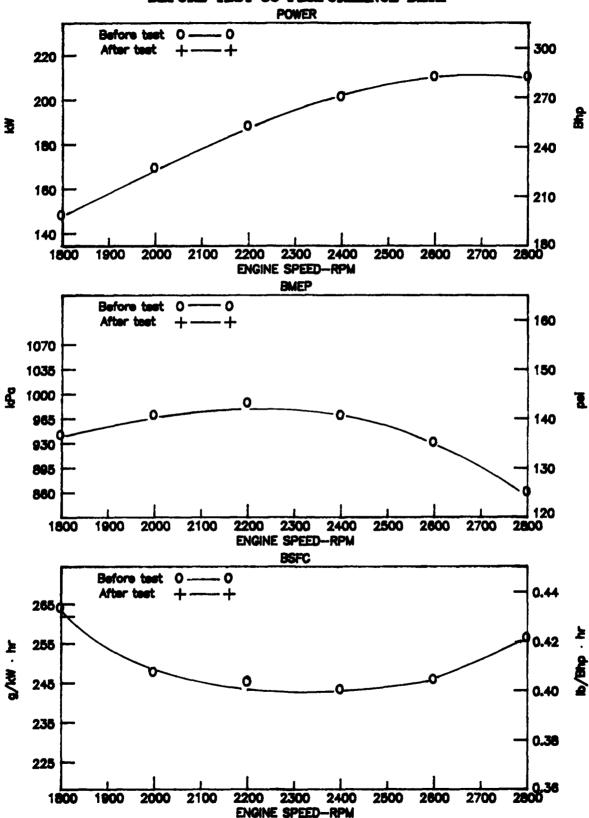
*Test stopped at 20 hours due to severe cylinder liner scuffing and high Fe content in the oil.

6V-53T
TEST 35
ENGINE REBUILD MEASUREMENTS*
Model Number: 5063-5395
Serial Number: 6D-178671

	Min	<u>Max</u>	Avg	Specified Limits	
Cylinder Block Bore					
Inside Diameter (Bottom)	4.3571(110.670)	4.3588(110.714)	4.3580(110.693)	4.3565(110.655)	- 4.3575(110.681) Ne - 4.3595(110.731) Ma
Out-of-Round Taper	0.0001(0.003) 0.0001(0.003)	0.0019(0.048) 0.0010(0.025)	0.0009(0.023) 0.0008(0.020)		- 0.0015(0.038) Max - 0.0015(0.038) Max
Cylinder Liners (Installed)					
Inside Dismeter Out-of-Round	3.8758(98.445) 0.0000	3.8768(98.471) 0.0006(0.015)	3.8762(98.455) 0.0002(0.005)	3.8752(98.430)	- 3.8767(98.468) - 0.0015(0.038) Max
Taper	0.0001(0.003)	0.0006(0.015)	0.0003(0.008)		- 0.0015(0.038) Max
Piston Diameter (at skirt)	3.8675(98.23)	3.8681 (98.250)	3.8678(98.242)	3.8669(98.219)	- 3.8691(98.775)
Piston Skirt to Cylinder Liner Clearance	0.0078(0.198)	0.0089(0.226)	0.0084(0.213)	0.0061(0.155)	- 0.0098(0.249)
Compression Rings Gap (No. 1, Fire Ring) Gap (Nos. 2, 3, 4)	0.030(0.76) 0.028(0.71)	0.033(0.84) 0.034(0.86)	0.032(0.81) 0.030(0.76)	0.020(0.51) 0.020(0.51)	- 0.046(1.17) - 0.036(0.91)
Ring-to-Groove Clearance** Top (No. 1, Fire Ring) No. 2, Compression Ring No. 3 and 4, Compression Rings	0.003(0.08) 0.007(0.18) 0.006(0.15)	0.004(0.10) 0.008(0.20) 0.006(0.15)	0.004(0.10) 0.008(0.20) 0.006(0.15)	0.003(0.08) 0.007(0.18) 0.005(0.13)	- 0.006(0.15) - 0.010(0.25) - 0.003(0.20)
Nos. 5, 6, 7 Gap Ring-to-Groove Clearance	0.012(0.30) 0.002(0.05)	0.016(0.41) 0.004(0.10)	0.013(0.33) 0.003(0.08)	0.010(0.25) 0.0015(0.038)	- 0.025(0.64) - 0.0055(0.140)
Piston Pin Pin-to-Piston Bushing Clearance	0.0029(0.074)	0.0032(0.081)	0.0031(0.079)	0.0025(0.064)	- 0.0034(0.086)
Pin-to-Connecting Rod Bushing Clearance	0.0015(0.038)	0.0019(0.048)	0.0017(0.043)	0.0010(0.025)	- 0.0019(0.048)
Connecting Rod Bearing- to-Journal Clearance	0.0013(0.033)	0.0021(0.053)	0.0018(0.046)	0.0011(0.028)	- 0.00-1(0.1)-/
Main Bearing-to-Journal Clearance	Not measured				
Camshaft Bearing-to- Journal Clearance	Not measured				

^{*} Measurement is in inches and (mm).

6V-53T 240-HOUR TRACKED VEHICLE CYCLE HEFORE TEST 35 PERFORMANCE DATA



6V-53T 240-HOUR TRACKED VEHICLE CYCLE ENDURANCE TEST TEST 35 OPERATING CONDITIONS SUMMARY

Lubricant: AL-12186-L Fuel: Caterpillar 1-H

	Maximum Power Mode (2800 RPM)		Maximum To (2200	orque Mode RPM)
		Standard		Ständard
	Mean	<u>Deviation</u>	Mean	Deviation
Engine Speed, rpm	2800	4.18	2200	3.58
Torque, ft-lb (N-m)	442(599)	2.36(3.19)	498 (675)	2.77(3.74)
Fuel Consumption, lb/hr(kg/hr)	97.2(44.1)	1.76(0.80)	81.1(36.8)	0.77(0.35)
Observed Power, Bhp(kW)	235 (176)	1.46(1.09)	208 (156)	1.10(0.82)
BSFC, 1b/Bhp-hr(g/kW-hr)	0.413(251)	0.007(4.25)	0.390(237)	0.005(2.98)
Temperatures, °F(°C)				
Exhaust before Turbo	842(450)	20.90(11.6)	817(436)	20.8(11.5)
Exhaust after Turbo	710(377)	16.60(9.23)	709 (376)	23.6(13.1)
Water Jacket Inlet	159 (70.5)	0.60(0.34)	159 (70.5)	0.67(0.37)
Water Jacket Outlet	170(76.8)	0.45(0.25)	169 (76.3)	0.86(0.48)
Oil Sump	223(106)	1.57(0.87)	213(101)	2.91(1.62)
Fuel at Filter	92.7(33.7)	4.19(2.33)	88.3(31.3)	1.32(0.73)
Inlet Air	91.2(32.9)	3.44(1.91)	90.3(32.4)	3.17(1.76)
Airbox	255.7(124)	3.42(1.90)	210(99)	3.50(1.95)
Pressures				
Exhaust before Turbo,				
psi(kPa)	10.81 (74.5)	0.09(0.64)	6.98(48.1)	0.09(0.64)
Exhaust after Turbo,				
in. Hg(kPa)	2.62(8.84)	0.04(0.15)	1.55(5.23)	0.03(0.09)
Compressor Discharge, psi(kPa)	11.18(77.1)	0.06(0.39)	7.99(55.1)	0.06(0.39)
Blower Discharge, psi(kPa)	16.65(115.0)	0.34(2.33)	9.98(68.8)	0.09(0.63)
Oil Gallery, psi (kPa)	49.69(343)	0.15(1.01)	42.10(290)	0.28(1.90)
Intake Vacuum, in. H ₂ 0(kPa)	6.60(1.64)	0.09(0.02)	3.80(0.95)	0.05(0.01)
Ambient Conditions				
Dry Bulb Temperature, °F(°C)	77.58(25.3)	4.08(2.27)	77.4(25.2)	3.44(1.91)
Wet Bulb Temperature, °F(°C) Barometric Pressure,	75.76(24.3)	5.49(3.05)	75.3(24.0)	4.61(2.56)
in. Hg(kPa) (Both modes of operation)	29.04(98.06)	0.07(0.02)		

^{*68%} of the values for a given variable occur within ±1 standard deviation of the mean; 95% occur within ±2 standard deviations.

6V-53T TEST 35 LUBRICANT ANALYSIS Lubricant: AL-12186-L

	ASTM Test <u>Method</u>	Test Ti	me, Hours
Kinematic viscosity at 40°C (104°F) cSt	D 445	33.89	
Kinematic viscosity at 100°C (212°F) cSt	D 445	5.69	5.83
Total Acid Number mg KOH/g	D 664	1.57	
Total Base Number mg KOH/g	D 664	3.61	-
Pentane B Insclubles wt%	D 893	0.00	
Toluene B Insolubles wt%	D 893	0.00	
Flash Point, °C	D 92	221	

TOTAL CONSUMPTION AND WEAR METALS BY XRF

Test Time, Hours	Total Oil Consumed, 1b(kg)	Wear Me	tals, ppm
		Fe	Cu
0		< 10	< 10
20	9.74 (4.42)	320	11

Average oil consumption rate: 0.49 lb/hr (0.22 kg/hr)

6V-53T TEST 35 Lubricant: AL-12186-L

WEAR MEASUREMENTS*

Cylinder Liner Bore Diameter Change

		1.	<u>3L</u>			
	<u>T-AT**</u> <u>F-B</u>		<u>T-AT</u> <u>F-B</u>		T-AT F-B	
Top Middle Fottom	+0.0031 (0.079) +0.0013 (0.033) +0.0003 (0.008)	-0.0001 (-0.003) +0.0007 (0.018) +0.0004 (0.010)	+0.6012 (0.030) +0.0005 (0.013) +0.0002 (0.005)	-0.0002 (-0.005) 0.0000 +0.0002 (0.005)	+0.0033 (0.084 +0.0017 (0.043 +0.0001 (0.003	+0.0010 (0.025)
	<u>1R</u>		Cylinder Number 2R		<u>3r</u>	
	T-AT*	<u>F-B</u>	T-AT	<u>F-B</u>	<u>T-AT</u>	<u>F-B</u>
lop Middle Bottom	+0.0008(0.920) -0.0001(-0.003) +0.0003(0.008) +0.0002(0.005) +0.0001(0.003) +0.0003(0.008)		+0.0023(0.058) +0.0010(0.025) +0.0018(0.046) +0.0012(0.030) +0.0000 +0.0002(0.005)		+0.0014(0.036) +0.0006(0.015) +0.0002(0.005)	-0.0004(-0.010) -0.0001(-0.003) +0.0002(0.005)

Average Change

	<u>T-AT</u>	<u>F-B</u>		
Top Middle	+0.0020 (0.051) +0.0010 (0.025)	+0.0005 (0.013) +0.0005 (0.013)		
Bottom	+0.0002 (0.005)	+0.0003 (0.008)		

Overall average change: +0.0008 (0.020)

Piston Ring End Gap Change

Ring Number	<u>1L</u>	<u>2L</u>	<u>3L</u>	<u>1R</u>	<u>2R</u>	<u>3R</u>	Average Change
1	+0.009(0.23)	+0.003(0.08)	+0.008(0.20)	+0.004(0.10)	+0.039(0.99)	+0.004(0.10)	+0.011(0.28)
2	+0.004(0.10)	+0.003(0.08)	+0.003(0.08)	+0.002(0.05)	+0.007(0.18)	+0.003(0.08)	+0.004(0.10)
3	+0.001(0.03)	+0.003(0.08)	+0.002(0.05)	+0.002(0.05)	+0.004(0.10)	+0.001(0.03)	+0.002(0.05)
4	+0.001(0.03)	+0.003(0.08)	+0.002(0.05)	+0.001(0.03)	+0.005(0.13)	0.000	+0.002(0.05)
5	+0.041(1.04)	+0.009(0.23)	+0.145(3.68)	+0.010(0.25)	+0.130(3.30)	+0.008(0.20)	+0.057(1.45)
6	+0.018(0.46)	+0.008(0.20)	+0.083(2.10)	+0.006(0.15)	+0.016(0.41)	+0.007(0.18)	+0.023(0.58)
7	+0.019(0.48)	+0.009(0.23)	+0.084(2.13)	+0.008(0.20)	+0.017(0.43)	+0.007(0.18)	+0.024(0.61)

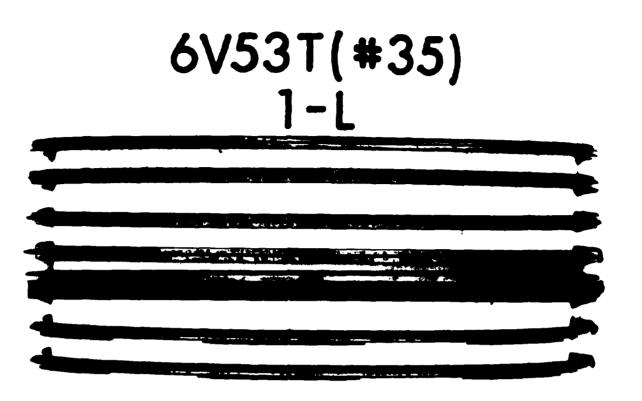
Overall average change: +0.018(0.46)

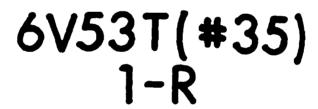
^{*1!} dimensions are given in inches (mm).
**I-AI = Thrust-Antithrust Direction; F-B = Front-Back Direction.

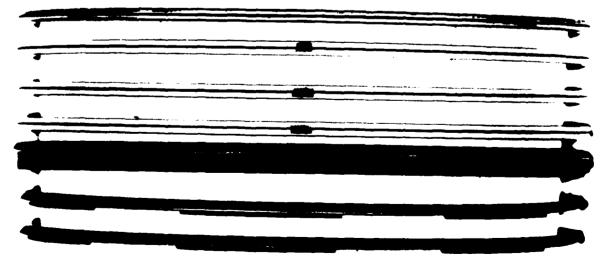
6V-53T TEST 35 Lubricant: AL-12186-L POST TEST ENGINE CONDITION AND DEPOSITS

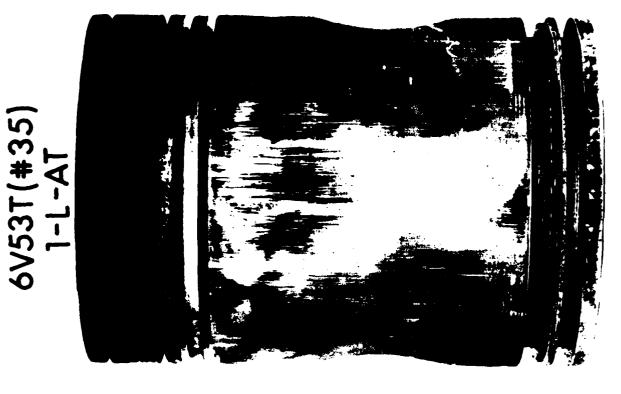
	1L	2L	3L	1R	2R	3R	Average A.			
Cylinder Liner										
Intake Port Plugging, Z restriction	< 1	< 1	< 1	< 1	< 1	< 1	< 1			
Liner Scuffing,										
Thrust Anti-Thrust Z Total Area Scuffed	100 86 93	12 0 6	100 83 91.5	1 12 6.5	100 100 100	16 1 8.5 Overall:	54.83 47.00 50.92 50.92			
I Area Bore Polished Thrust	0	2	0	2	0	2	1.00			
Anti-Thrust	Ö	i	0	2	0	1	0.67			
X Avg. Area Bore Polished	0	1.5	0	2	0	1.5 Overall:	0.83 0.83			
B. Pistons										
Ring Face Distress, (demerits)										
No. 1	66.25	34.00	28.75	21.00 0.25	72.50	32.50 12.50	42.50 30.88			
No. 2 No. 3	58.25 55.50	33.00 40.00	32.50 28.75	0.00	48.75 51.75	13.50 Overall:	31.58 34.99			
Piston Skirt Rating Thrust	95 2 5C*	15 % SC	95 % SC	5%SC	25%PM/	5 % 5C				
Anti-Thrust	35 % SC	5 XSC	80 % SC	5 % SC	80%SC 65%SC	s				
Piston WTD Rating**	151.63	126.38	147.5	131.00	179.00	148.63	147.36			
Ring Sticking						_				
No. 1	F F	F F	F F	P F	CO### F	F F				
No. 2 No. 3	F	F	F	F	F	F				
No. 4	F	F	F	P	F	F				
C. Exhaust Valves										
Deposits Head				_1/4 AHC+	·					
Face	-			_1 /4 AHC		-				
Tulip	-			_1/4 AHC						
Stem	4	-	1/4 Ai	IC EO PY	Lacquer					
Surface Condition Freeness in Guide	P	F	P	P	F	F				
Head				_ Normal _		-				
Face	4			-Normal-		-				
Seat Stem				- Normal-		-				
Tip	-			Normal_		-				
D. Other Ratings										
Upper Oil Control Ring Expansive Force, 1bs.	19.6	20,2	19.8	19.8	19.2	19.0	19.6			
Main Bearings / 2 main bearing has scratches and metal flaking Rod Journals Scratched Tappets, Came										
and Rocker Arm Condition	Cam lobe	Cam lobes show light to medium wear with scratches								

^{*}L = Light, S = Scratches, PM = Plating Melted, N = Normal, SC = Scuffing, B = Burn
**CRC Weighted Total Deposits (0 = least, 900 = most)
***AS = Hotstuck, CS = Cold Stuck, P = Pinched, F = Free, N = Normal, C = Chipped,
CO = Collapsed
+HC = Hard Carbon; the number-letter, prefix indicates carbon depth with 1/4 A = least
to J = most
++ = The higher the number, the darker the lacquer (0 = lightest, 9 = darkest)









6V53T(#35)]-L-T

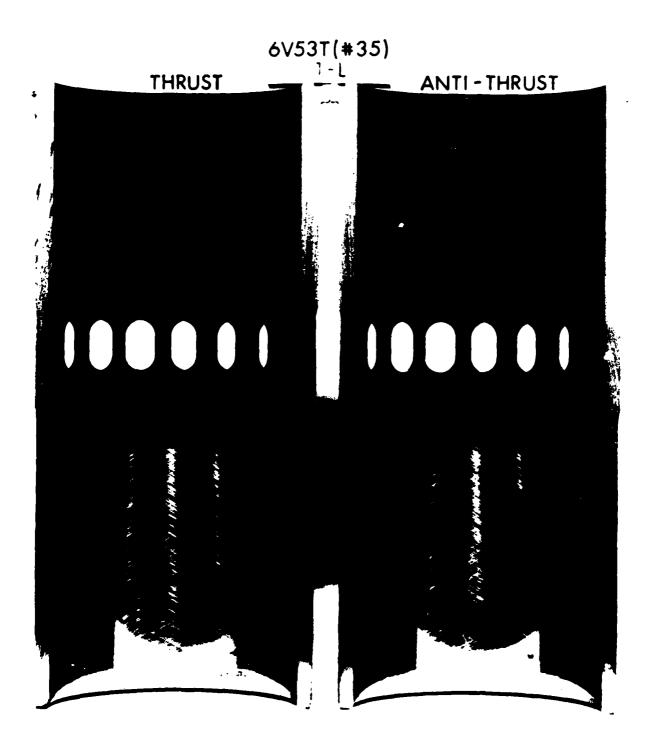


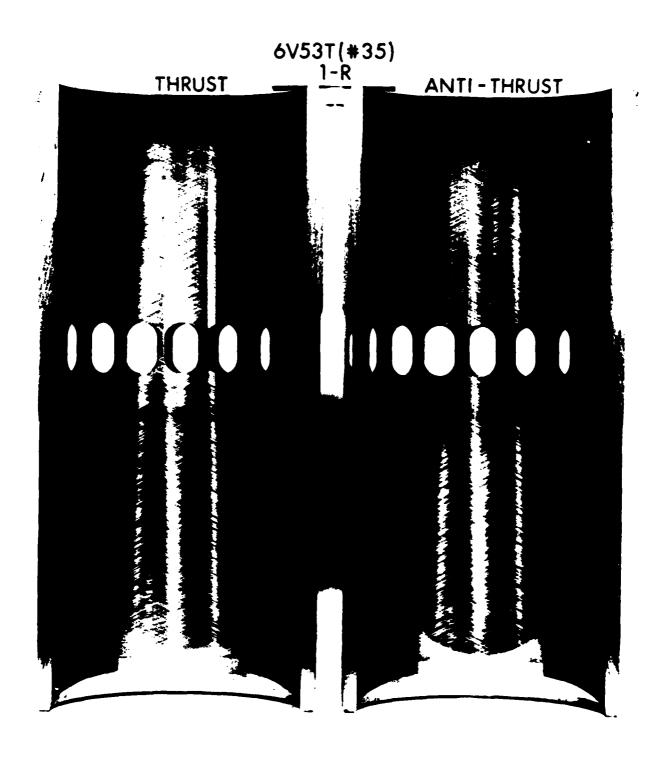
1-R-AT

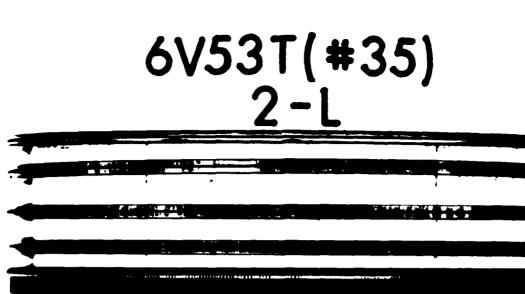
6V53T(#35) 1-R-T

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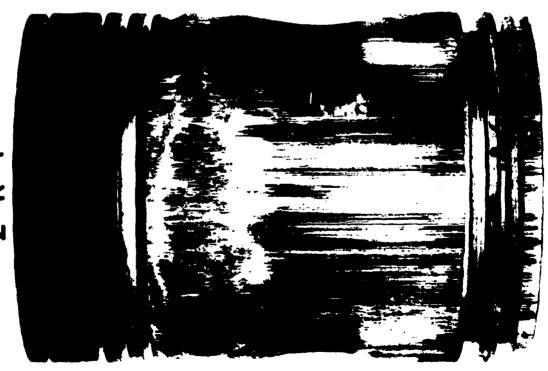


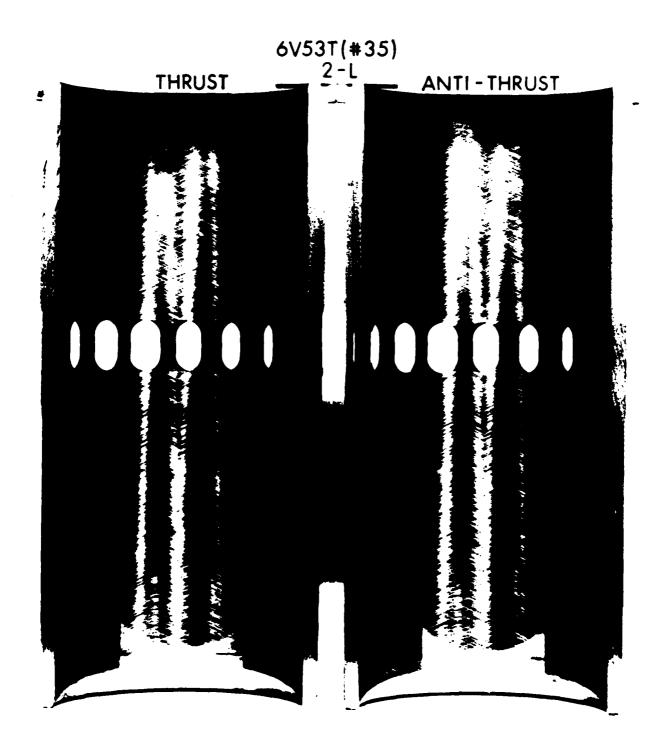
E-14

6V53T(#35) 2-R-AT

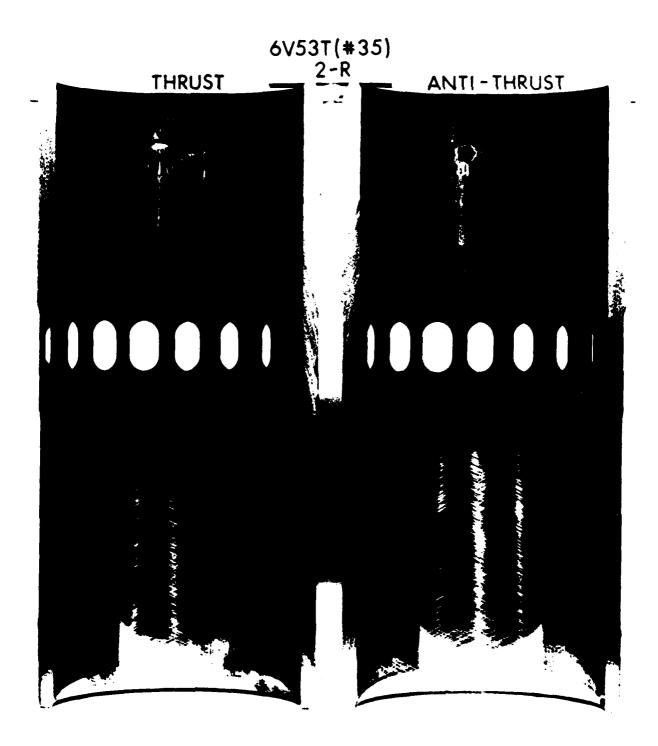
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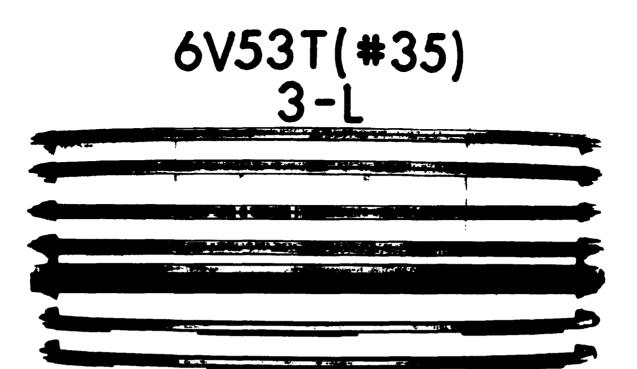
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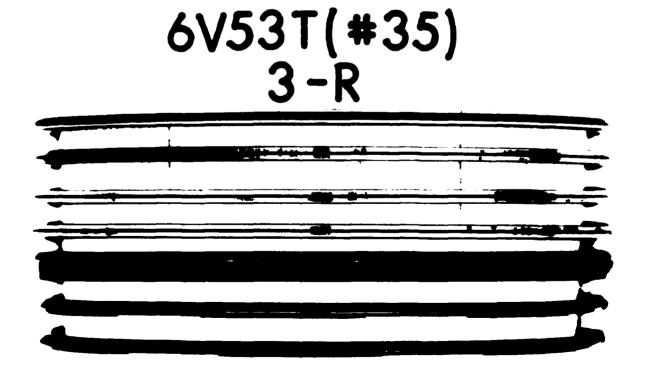


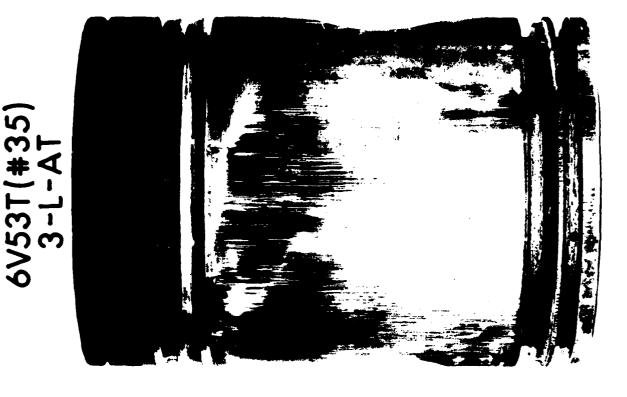


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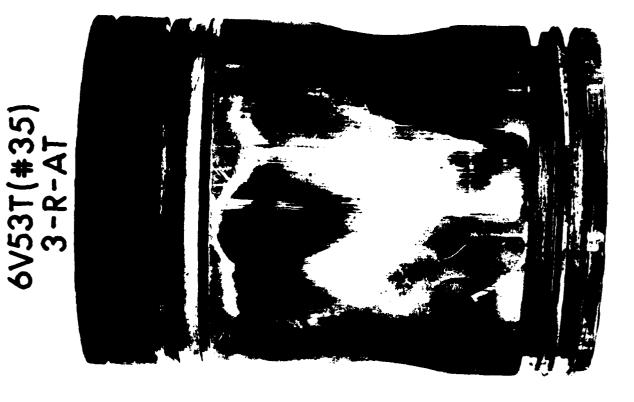




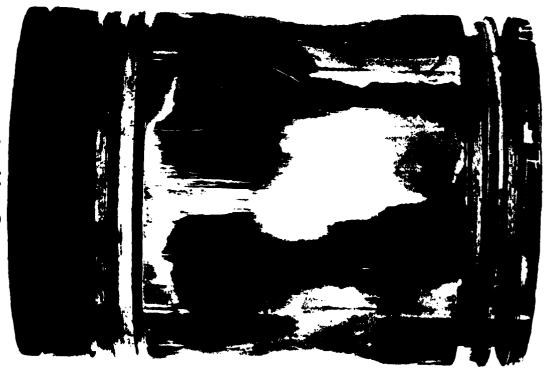


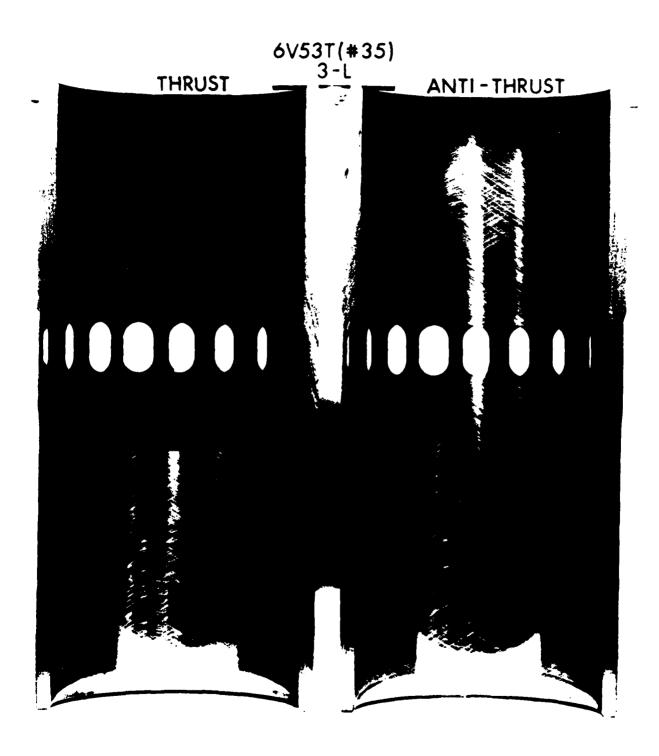
6V53T(#35) 3-L-T



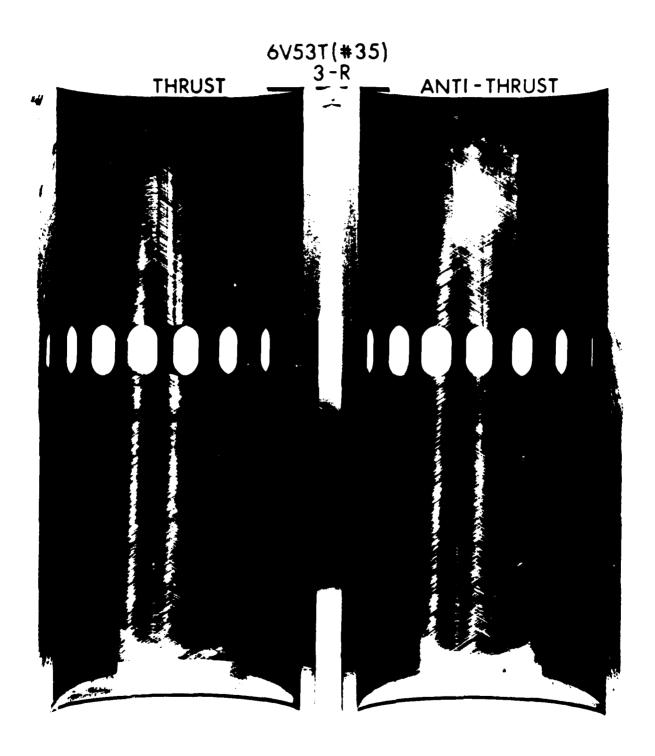


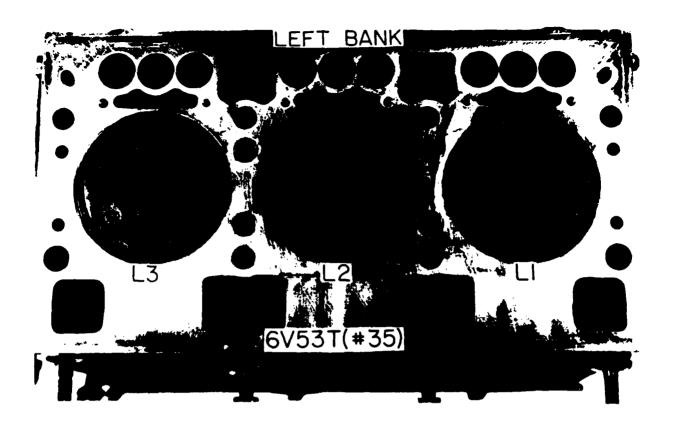
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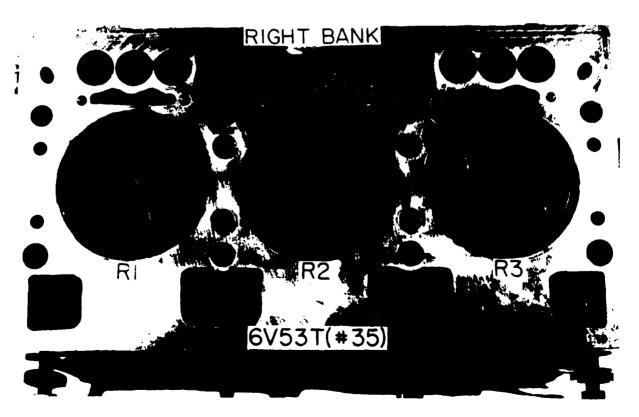




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